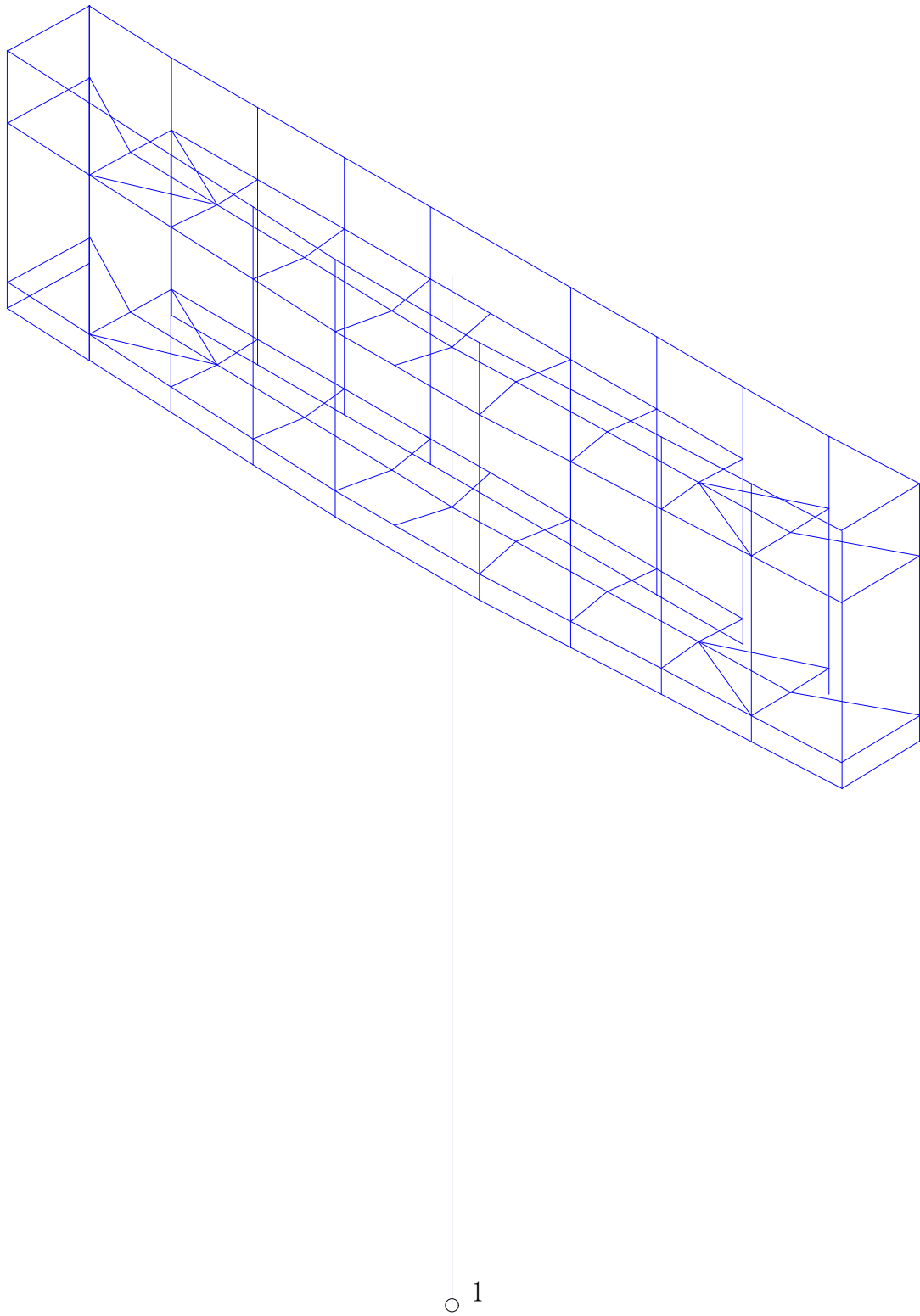
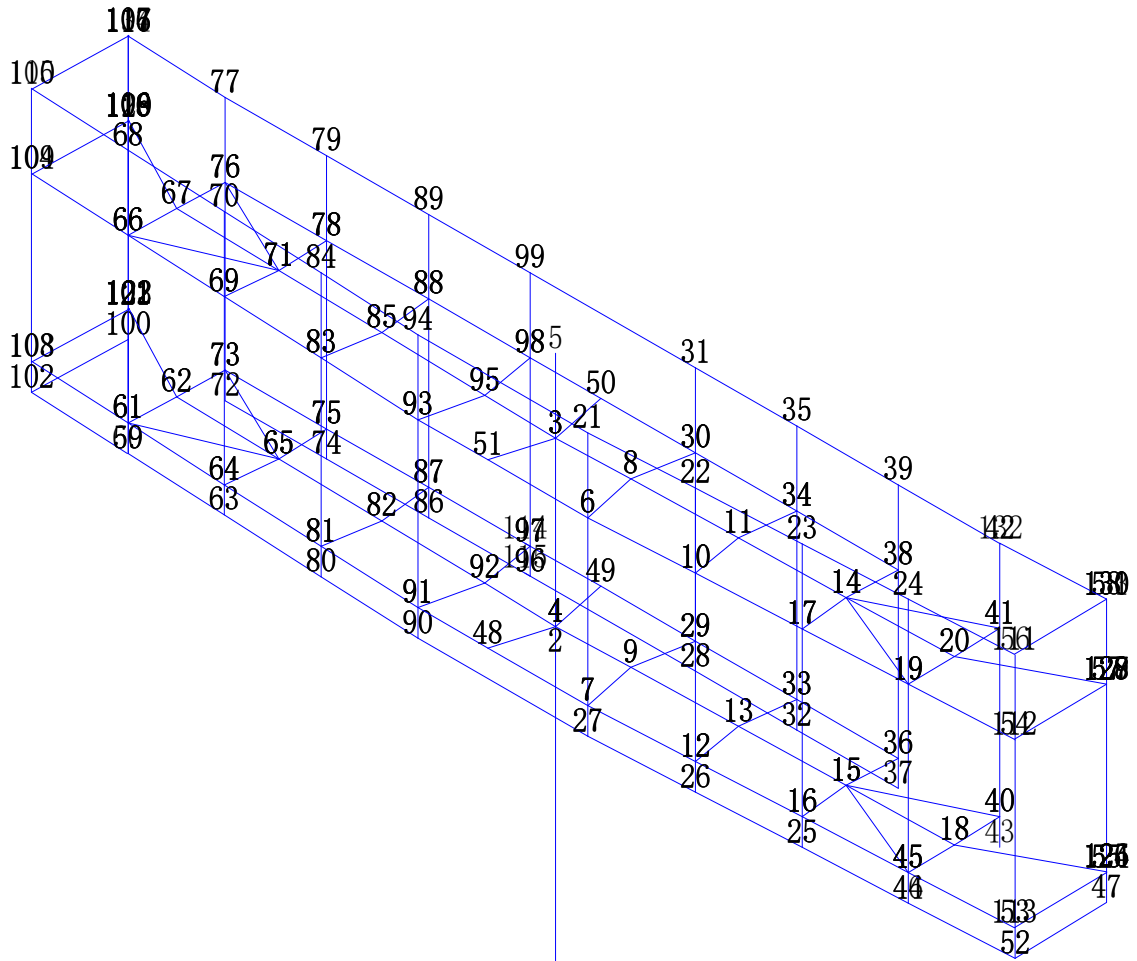


工 程 名：
设 计 单 位：
计 算 人：
计 算 时 间：
工 程 负 责 人：
检 查：
审 核：

一、计算简图

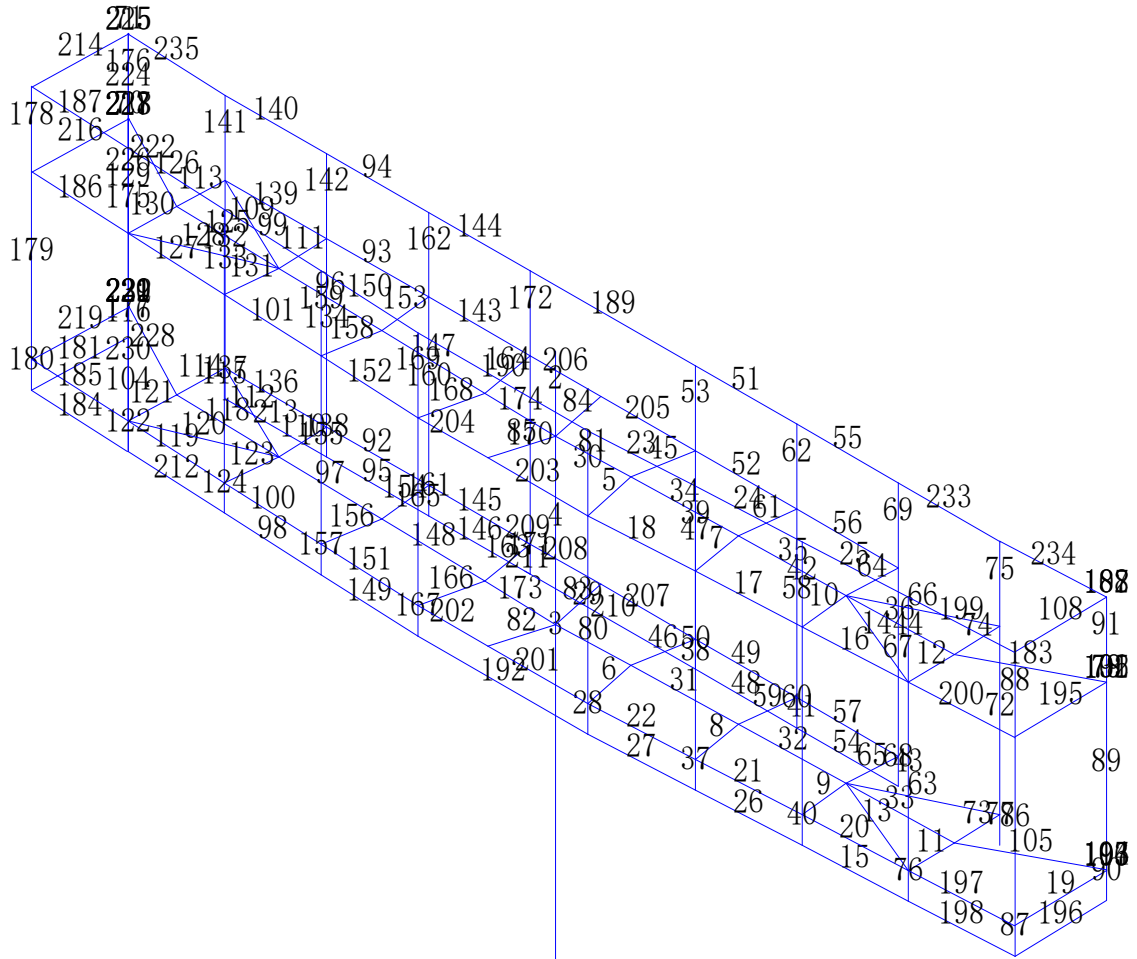


计算简图 (圆表示支座, 数字为节点号)



1

节点编号图



1

单元编号图

二、几何信息

各节点信息如下表:

节点号	x坐标 (m)	y坐标 (m)	z坐标 (m)	x向 约束	y向 约束	z向 约束	绕x 约束	绕y 约束	绕z 约束
1	5.657	-6.288	-0.004	i	i	i	i	i	i
2	5.657	-6.288	14.996						
3	5.657	-6.288	18.596						
4	5.657	-6.288	15.496						
5	5.657	-6.288	19.996						
6	7.271	-7.290	18.596						
7	7.271	-7.290	15.496						
8	7.038	-6.253	18.596						
9	7.038	-6.253	15.496						
10	9.201	-7.191	18.596						
11	9.037	-6.202	18.596						
12	9.201	-7.191	15.496						
13	9.037	-6.202	15.496						
14	11.037	-6.152	18.596						
15	11.037	-6.152	15.496						
16	11.131	-7.093	15.496						
17	11.131	-7.093	18.596						
18	13.036	-6.101	15.496						
19	13.056	-6.995	18.596						
20	13.036	-6.101	18.596						
21	7.271	-7.290	19.996						
22	9.201	-7.191	19.996						
23	11.131	-7.093	19.996						
24	13.056	-6.995	19.996						
25	11.131	-7.093	14.996						
26	9.201	-7.191	14.996						
27	7.271	-7.290	14.996						
28	7.218	-5.206	14.996						
29	7.218	-5.206	15.496						
30	7.218	-5.206	18.596						
31	7.218	-5.206	19.996						
32	9.150	-5.206	14.996						

33	9.150	-5.206	15.496						
34	9.150	-5.206	18.596						
35	9.150	-5.206	19.996						
36	11.083	-5.206	15.496						
37	11.083	-5.206	14.996						
38	11.083	-5.206	18.596						
39	11.083	-5.206	19.996						
40	13.010	-5.206	15.496						
41	13.010	-5.206	18.596						
42	13.010	-5.206	19.996						
43	13.010	-5.206	14.996						
44	13.056	-6.995	14.996						
45	13.056	-6.995	15.496						
46	13.061	-6.995	14.996						
47	14.935	-5.108	14.996						
48	5.371	-7.290	15.496						
49	5.424	-5.206	15.496						
50	5.424	-5.206	18.596						
51	5.371	-7.290	18.596						
52	14.980	-6.897	14.996						
53	14.980	-6.897	15.496						
54	14.980	-6.897	18.596						
55	14.935	-5.108	15.496						
56	14.980	-6.897	19.996						
57	14.935	-5.108	18.596						
58	14.935	-5.108	19.996						
59	-1.742	-6.995	14.996						
60	-1.748	-6.995	14.996						
61	-1.742	-6.995	15.496						
62	-1.723	-6.101	15.496						
63	0.182	-7.093	14.996						
64	0.182	-7.093	15.496						
65	0.277	-6.152	15.496						
66	-1.742	-6.995	18.596						
67	-1.723	-6.101	18.596						
68	-1.742	-6.995	19.996						
69	0.182	-7.093	18.596						
70	0.182	-7.093	19.996						
71	0.277	-6.152	18.596						

72	-1.697	-5.206	14.996						
73	-1.697	-5.206	15.496						
74	0.230	-5.206	14.996						
75	0.230	-5.206	15.496						
76	-1.697	-5.206	18.596						
77	-1.697	-5.206	19.996						
78	0.230	-5.206	18.596						
79	0.230	-5.206	19.996						
80	2.113	-7.191	14.996						
81	2.113	-7.191	15.496						
82	2.276	-6.202	15.496						
83	2.113	-7.191	18.596						
84	2.113	-7.191	19.996						
85	2.276	-6.202	18.596						
86	2.163	-5.206	14.996						
87	2.163	-5.206	15.496						
88	2.163	-5.206	18.596						
89	2.163	-5.206	19.996						
90	4.043	-7.290	14.996						
91	4.043	-7.290	15.496						
92	4.276	-6.253	15.496						
93	4.043	-7.290	18.596						
94	4.043	-7.290	19.996						
95	4.276	-6.253	18.596						
96	4.096	-5.206	14.996						
97	4.096	-5.206	15.496						
98	4.096	-5.206	18.596						
99	4.096	-5.206	19.996						
100	-3.621	-5.108	14.996						
101	-3.621	-5.108	15.496						
102	-3.667	-6.897	14.996						
103	-3.667	-6.897	15.496						
104	-3.667	-6.897	18.596						
105	-3.667	-6.897	19.996						
106	-3.621	-5.108	18.596						
107	-3.621	-5.108	19.996						
108	-3.661	-6.898	15.496						
109	-3.661	-6.898	18.596						
110	-3.661	-6.898	19.996						

111	14.975	-6.898	19.996						
112	14.975	-6.898	18.596						
113	14.975	-6.898	15.496						
114	3.990	-5.206	15.496						
115	3.990	-5.206	14.996						
116	-3.616	-5.114	19.996						
117	-3.616	-5.109	19.996						
118	-3.616	-5.114	18.596						
119	-3.616	-5.111	18.596						
120	-3.616	-5.109	18.596						
121	-3.616	-5.114	15.496						
122	-3.616	-5.111	15.496						
123	-3.616	-5.109	15.496						
124	14.929	-5.114	15.496						
125	14.929	-5.111	15.496						
126	14.929	-5.109	15.496						
127	14.929	-5.114	18.596						
128	14.929	-5.111	18.596						
129	14.929	-5.109	18.596						
130	14.929	-5.114	19.996						
131	14.929	-5.109	19.996						
132	13.016	-5.206	19.996						
133	14.935	-5.108	19.996						
134	-3.616	-5.114	19.996						

各单元信息如下表:

单元号	截面名称	长度(m)	面积(mm ²)	绕2轴惯性矩(x10 ⁴ mm ⁴)	绕3轴惯性矩(x10 ⁴ mm ⁴)	绕2轴计算长度系数	绕3轴计算长度系数	小节点释放	大节点释放
1	ÈÈ, Ö' Ü1420x16	15.000	60520	1096822	1096822	1.000	1.000	---	---
2	ÈÈ, Ö' Ü1020x12	1.400	38001	482708	482708	1.000	1.000	---	---
3	ÈÈ, Ö' Ü1020x12	0.500	38001	482708	482708	1.000	1.000	---	---
4	ÈÈ, Ö' Ü1020x12	3.100	38001	482708	482708	1.000	1.000	---	---

5	Á° 200x100x5. 5x8	1.06 2	3144	254	3378	1.00 0	1.00 0	---	---
6	Á° 200x100x5. 5x8	1.06 2	3144	254	3378	1.00 0	1.00 0	---	---
7	Á° 200x100x5. 5x8	1.00 2	3144	254	3378	1.00 0	1.00 0	---	---
8	Á° 200x100x5. 5x8	1.00 2	3144	254	3378	1.00 0	1.00 0	---	---
9	Á° 200x100x5. 5x8	0.94 6	3144	254	3378	1.00 0	1.00 0	---	---
10	Á° 200x100x5. 5x8	0.94 6	3144	254	3378	1.00 0	1.00 0	---	---
11	Á° 200x100x5. 5x8	0.89 5	3144	254	3378	1.00 0	1.00 0	---	---
12	Á° 200x100x5. 5x8	0.89 5	3144	254	3378	1.00 0	1.00 0	---	---
13	Çá² Û14	2.18 8	1546	521	55	1.00 0	1.00 0	---	---
14	Çá² Û14	2.18 8	1546	521	55	1.00 0	1.00 0	---	---
15	Çá² Û14	1.92 7	6089	15867	800	1.00 0	1.00 0	---	---
16	Çá² Û14	1.92 7	1546	521	55	1.00 0	1.00 0	---	---
17	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
18	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
19	Çá² Û14	1.78 4	1546	521	55	1.00 0	1.00 3	---	---
20	Çá² Û14	1.92 7	1546	521	55	1.00 0	1.00 0	---	---
21	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
22	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
23	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
24	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---

25	Çá² Û14	1.92 7	6089	15867	800	1.00 0	1.00 0	---	---
26	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
27	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
28	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
29	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
30	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
31	ÈÈ, Ö¹ Ü530x10	2.00 0	1633 6	55237	55237	1.00 0	1.00 0	---	---
32	ÈÈ, Ö¹ Ü530x10	2.00 0	1633 6	55237	55237	1.00 0	1.00 0	---	---
33	ÈÈ, Ö¹ Ü530x10	2.00 0	1633 6	55237	55237	1.00 0	1.00 0	---	---
34	ÈÈ, Ö¹ Ü530x10	2.00 0	1633 6	55237	55237	1.00 0	1.00 0	---	---
35	ÈÈ, Ö¹ Ü530x10	2.00 0	1633 6	55237	55237	1.00 0	1.00 0	---	---
36	ÈÈ, Ö¹ Ü530x10	2.00 0	1633 6	55237	55237	1.00 0	1.00 0	---	---
37	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
38	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
39	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
40	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
41	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
42	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
43	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
44	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---

45	Á° 200x100x5. 5x8	1.06 2	3144	254	3378	1.00 0	1.00 0	---	---
46	Á° 200x100x5. 5x8	1.06 2	3144	254	3378	1.00 0	1.00 0	---	---
47	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
48	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
49	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
50	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
51	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
52	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
53	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
54	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
55	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
56	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
57	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
58	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
59	Á° 200x100x5. 5x8	1.00 2	3144	254	3378	1.00 0	1.00 0	---	---
60	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
61	Á° 200x100x5. 5x8	1.00 2	3144	254	3378	1.00 0	1.00 0	---	---
62	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
63	Çá² Û14	2.18 8	1546	521	55	1.00 0	1.00 0	---	---
64	Á° 200x100x5. 5x8	0.94 6	3144	254	3378	1.00 0	1.00 0	---	---

65	Á° 200x100x5. 5x8	0.94 6	3144	254	3378	1.00 0	1.00 0	---	---
66	Çá² Û14	2.18 8	1546	521	55	1.00 0	1.00 0	---	---
67	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
68	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
69	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
70	Çá² Û14	0.00 6	1546	521	55	1.00 0	1.00 0	---	---
71	Çá² Û14	0.00 6	6089	15867	800	1.00 0	1.00 0	---	---
72	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
73	Á° 200x100x5. 5x8	0.89 5	3144	254	3378	1.00 0	1.00 0	---	---
74	Á° 200x100x5. 5x8	0.89 5	3144	254	3378	1.00 0	1.00 0	---	---
75	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
76	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
77	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
78	Çá² Û14	0.00 3	1546	521	55	1.00 0	692. 592	---	---
79	Çá² Û14	0.00 3	1546	521	55	1.00 0	694. 958	---	---
80	ÈÈ, Ö¹ Ü530x10	1.38 2	1633 6	55237	55237	1.00 0	1.00 0	---	---
81	ÈÈ, Ö¹ Ü530x10	1.38 2	1633 6	55237	55237	1.00 0	1.00 0	---	---
82	Á° 200x100x5. 5x8	1.04 1	3144	254	3378	1.00 0	1.00 0	---	---
83	Á° 200x100x5. 5x8	1.10 7	3144	254	3378	1.00 0	1.00 0	---	---
84	Á° 200x100x5. 5x8	1.10 7	3144	254	3378	1.00 0	1.00 0	---	---

85	Á° 200x100x5. 5x8	1.04 1	3144	254	3378	1.00 0	1.00 0	---	---
86	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
87	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
88	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
89	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
90	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
91	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
92	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
93	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
94	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
95	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
96	ÈÈ, Ö¹ Ü530x10	2.00 0	1633 6	55237	55237	1.00 0	1.00 0	---	---
97	ÈÈ, Ö¹ Ü530x10	2.00 0	1633 6	55237	55237	1.00 0	1.00 0	---	---
98	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
99	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
100	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
101	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
102	Çá² Û14	0.00 8	1546	521	55	1.00 0	1.00 0	---	---
103	ÈÈ, Ö¹ Ü530x10	0.00 6	1633 6	55237	55237	1.00 0	1.00 0	---	---
104	Çá² Û14	2.66 3	6089	15867	800	1.00 0	1.00 0	---	---

105	ÈÈ, Ö' Ü530x10	2.13 6	1633 6	55237	55237	1.00 0	1.00 0	---	---
106	Çá² Û14	0.00 8	1546	521	55	1.00 0	1.00 0	---	---
107	Çá² Û14	0.00 5	6089	15867	800	1.00 0	346. 886	---	---
108	Çá² Û14	1.78 4	6089	15867	800	1.00 0	1.00 3	---	---
109	Çá² Û14	2.18 8	1546	521	55	1.00 0	1.00 0	---	---
110	Á° 200x100x5. 5x8	0.94 6	3144	254	3378	1.00 0	1.00 0	---	---
111	Á° 200x100x5. 5x8	0.94 6	3144	254	3378	1.00 0	1.00 0	---	---
112	Çá² Û14	2.18 8	1546	521	55	1.00 0	1.00 0	---	---
113	Á° 200x100x5. 5x8	0.89 5	3144	254	3378	1.00 0	1.00 0	---	---
114	Á° 200x100x5. 5x8	0.89 5	3144	254	3378	1.00 0	1.00 0	---	---
115	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
116	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
117	Çá² Û14	0.00 6	1546	521	55	1.00 0	1.00 0	---	---
118	ÈÈ, Ö' Ü530x10	2.00 0	1633 6	55237	55237	1.00 0	1.00 0	---	---
119	Çá² Û14	1.92 7	1546	521	55	1.00 0	1.00 0	---	---
120	Çá² Û14	2.18 8	1546	521	55	1.00 0	1.00 0	---	---
121	Á° 200x100x5. 5x8	0.89 5	3144	254	3378	1.00 0	1.00 0	---	---
122	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
123	Á° 200x100x5. 5x8	0.94 6	3144	254	3378	1.00 0	1.00 0	---	---
124	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---

125	ÈÈ, Ö' Ü530x10	2.00 0	1633 6	55237	55237	1.00 0	1.00 0	---	---
126	Çá² Û14	1.92 7	6089	15867	800	1.00 0	1.00 0	---	---
127	Çá² Û14	1.92 7	1546	521	55	1.00 0	1.00 0	---	---
128	Çá² Û14	2.18 8	1546	521	55	1.00 0	1.00 0	---	---
129	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
130	Á° 200x100x5.5x8	0.89 5	3144	254	3378	1.00 0	1.00 0	---	---
131	Á° 200x100x5.5x8	0.94 6	3144	254	3378	1.00 0	1.00 0	---	---
132	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
133	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
134	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
135	ÈÈ, Ö' Ü530x10	0.00 6	1633 6	55237	55237	1.00 0	1.00 0	---	---
136	Çá² Û14	1.92 7	1546	521	55	1.00 0	1.00 0	---	---
137	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
138	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
139	Çá² Û14	1.92 7	1546	521	55	1.00 0	1.00 0	---	---
140	Çá² Û14	1.92 7	6089	15867	800	1.00 0	1.00 0	---	---
141	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
142	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
143	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
144	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---

145	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
146	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
147	ÈÈ, Ö¹ Ü530x10	2.00 0	1633 6	55237	55237	1.00 0	1.00 0	---	---
148	ÈÈ, Ö¹ Ü530x10	2.00 0	1633 6	55237	55237	1.00 0	1.00 0	---	---
149	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
150	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
151	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
152	Çá² Û14	1.93 3	1546	521	55	1.00 0	1.00 0	---	---
153	Á° 200x100x5. 5x8	1.00 2	3144	254	3378	1.00 0	1.00 0	---	---
154	Á° 200x100x5. 5x8	1.00 2	3144	254	3378	1.00 0	1.00 0	---	---
155	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
156	Á° 200x100x5. 5x8	1.00 2	3144	254	3378	1.00 0	1.00 0	---	---
157	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
158	Á° 200x100x5. 5x8	1.00 2	3144	254	3378	1.00 0	1.00 0	---	---
159	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
160	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
161	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
162	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
163	Á° 200x100x5. 5x8	1.06 2	3144	254	3378	1.00 0	1.00 0	---	---
164	Á° 200x100x5. 5x8	1.06 2	3144	254	3378	1.00 0	1.00 0	---	---

165	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
166	Á° 200x100x5.5x8	1.06 2	3144	254	3378	1.00 0	1.00 0	---	---
167	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
168	Á° 200x100x5.5x8	1.06 2	3144	254	3378	1.00 0	1.00 0	---	---
169	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
170	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
171	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
172	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
173	ÈÈ, Ö¹ Û530x10	1.38 2	1633 6	55237	55237	1.00 0	1.00 0	---	---
174	ÈÈ, Ö¹ Û530x10	1.38 2	1633 6	55237	55237	1.00 0	1.00 0	---	---
175	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
176	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
177	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
178	Çá² Û14	1.40 0	6089	15867	800	1.00 0	1.00 0	---	---
179	Çá² Û14	3.10 0	6089	15867	800	1.00 0	1.00 0	---	---
180	Çá² Û14	0.50 0	6089	15867	800	1.00 0	1.00 0	---	---
181	Çá² Û14	1.78 9	6089	15867	800	1.00 0	1.00 0	---	---
182	Çá² Û14	0.00 8	6089	15867	800	1.00 0	1.00 0	---	---
183	ÈÈ, Ö¹ Û530x10	2.13 6	1633 6	55237	55237	1.00 0	1.00 0	---	---
184	Çá² Û14	1.92 2	6089	15867	800	1.00 0	1.00 0	---	---

185	Çá² Û14	1.92 2	1546	521	55	1.00 0	1.00 0	---	---
186	Çá² Û14	1.92 2	1546	521	55	1.00 0	1.00 0	---	---
187	Çá² Û14	1.92 2	6089	15867	800	1.00 0	1.00 0	---	---
188	Çá² Û14	0.00 6	6089	15867	800	1.00 0	1.00 0	---	---
189	Çá² Û14	3.12 2	6089	15867	800	4.71 3	1.00 0	---	---
190	Çá² Û14	3.22 8	6089	15867	800	1.00 0	1.00 0	---	---
191	Çá² Û14	0.00 6	1546	521	55	1.00 0	1.00 0	---	---
192	Çá² Û14	3.22 8	6089	15867	800	1.00 0	1.00 0	---	---
193	Çá² Û14	0.00 3	1546	521	55	1.00 0	694. 958	---	---
194	Çá² Û14	0.00 3	1546	521	55	1.00 0	692. 592	---	---
195	Çá² Û14	1.78 4	1546	521	55	1.00 0	1.00 3	---	---
196	Çá² Û14	1.78 9	6089	15867	800	1.00 0	1.00 0	---	---
197	Çá² Û14	1.92 2	1546	521	55	1.00 0	1.00 0	---	---
198	Çá² Û14	1.92 2	6089	15867	800	1.00 0	1.00 0	---	---
199	Çá² Û14	1.92 2	6089	15867	800	4.01 4	1.00 0	---	---
200	Çá² Û14	1.92 2	1546	521	55	1.00 0	1.00 0	---	---
201	Çá² Û14	1.90 0	1546	521	55	1.00 0	1.69 9	---	---
202	Çá² Û14	1.32 8	1546	521	55	1.00 0	2.43 1	---	---
203	Çá² Û14	1.90 0	1546	521	55	1.00 0	1.69 9	---	---
204	Çá² Û14	1.32 8	1546	521	55	1.00 0	2.43 1	---	---

205	Çá² Û14	1.79 4	1546	521	55	1.00 0	1.74 0	---	---
206	Çá² Û14	1.32 8	1546	521	55	1.00 0	2.35 1	---	---
207	Çá² Û14	1.79 4	1546	521	55	1.00 0	1.74 0	---	---
208	Çá² Û14	1.32 8	1546	521	55	1.00 0	2.35 1	---	---
209	Çá² Û14	0.10 6	1546	521	55	1.00 0	1.00 0	---	---
210	Çá² Û14	3.12 2	6089	15867	800	2.27 2	1.00 0	---	---
211	Çá² Û14	0.10 6	6089	15867	800	66.9 70	1.00 0	---	---
212	Çá² Û14	1.92 7	6089	15867	800	1.00 0	1.00 0	---	---
213	Çá² Û14	1.92 7	6089	15867	800	1.00 0	1.00 0	---	---
214	Çá² Û14	1.78 4	6089	15867	800	1.00 0	1.00 3	---	---
215	Çá² Û14	0.00 5	6089	15867	800	1.00 0	346. 886	---	---
216	Çá² Û14	1.78 4	1546	521	55	1.00 0	1.00 3	---	---
217	Çá² Û14	0.00 3	1546	521	55	1.00 0	694. 958	---	---
218	Çá² Û14	0.00 3	1546	521	55	1.00 0	692. 592	---	---
219	Çá² Û14	1.78 4	1546	521	55	1.00 0	1.00 3	---	---
220	Çá² Û14	0.00 3	1546	521	55	1.00 0	694. 958	---	---
221	Çá² Û14	0.00 3	1546	521	55	1.00 0	692. 592	---	---
222	ÈÈ, Ö¹ Ü530x10	2.13 6	1633 6	55237	55237	1.00 0	1.00 0	---	---
223	ÈÈ, Ö¹ Ü530x10	0.00 6	1633 6	55237	55237	1.00 0	1.00 0	---	---
224	Çá² Û14	2.65 5	6089	15867	800	1.00 0	1.00 0	---	---

225	Çá² Û14	0.00 8	6089	15867	800	1.00 0	1.00 0	---	---
226	Çá² Û14	2.65 5	1546	521	55	1.00 0	1.00 0	---	---
227	Çá² Û14	0.00 8	1546	521	55	1.00 0	1.00 0	---	---
228	ÈÈ, Ö¹ Ü530x10	2.13 6	1633 6	55237	55237	1.00 0	1.00 0	---	---
229	ÈÈ, Ö¹ Ü530x10	0.00 6	1633 6	55237	55237	1.00 0	1.00 0	---	---
230	Çá² Û14	2.65 5	1546	521	55	1.00 0	1.00 0	---	---
231	Çá² Û14	0.00 8	1546	521	55	1.00 0	1.00 0	---	---
232	Çá² Û14	0.00 6	1546	521	55	1.00 0	1.00 0	---	---
233	Çá² Û14	1.93 3	6089	15867	800	1.00 0	1.00 0	---	---
234	Çá² Û14	1.92 7	6089	15867	800	1.00 0	1.00 0	---	---
235	Çá² Û14	1.92 1	6089	15867	800	1.00 0	1.00 0	---	---

三、荷载信息

(一). (恒、活、风) 节点、单元荷载信息

1. 节点荷载

**以下为节点荷载汇总表:

单位: 力(kN); 弯距(kN.m)

**以下为节点荷载图

单位: 力(kN); 弯距(kN.m)

2. 单元荷载

**以下为单元荷载汇总表:

单位: 力(kN); 分布力(kN/m); 弯距(kN.m); 分布弯距(kN.m/m)

μÚ 0 ¹ Ö¿öμ¥Öª°ÉÔØ±i

单元号	工况号	类型	方向	Q1	Q2	X1	X2
5	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.3	0.0
6	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.3	0.0
7	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.6	0.0
7	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.4	0.0
8	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.6	0.0
8	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.4	0.0
9	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.4	0.0
9	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.7	0.0
10	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.4	0.0
10	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.7	0.0
11	0	¾û² ¼° ÉÔØ	Z	-0.2	-0.2	0.0	0.0
11	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.3	0.0
12	0	¾û² ¼° ÉÔØ	Z	-0.2	-0.2	0.0	0.0
12	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.6	0.0
13	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.9	0.0
13	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
14	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.9	0.0
14	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
15	0	ÏÝÐÎ° ÉÔØ	Z	-0.1	-0.1	0.3	1.7
16	0	Ëý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.0	0.0
16	0	ÏÝÐÎ° ÉÔØ	Z	-0.2	-0.2	0.7	1.2
16	0	Ëý½ÇÐÎ°	Z	-0.1	0.0	0.6	0.0

		ÉÔØ					
17	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.0	0.0
17	0	ÌÝÐÎ° ÉÔØ	Z	-0.2	-0.2	0.7	1.2
17	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.0	0.0
18	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.0	0.0
18	0	ÌÝÐÎ° ÉÔØ	Z	-0.2	-0.2	0.7	1.2
18	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.9	0.0
20	0	ÌÝÐÎ° ÉÔØ	Z	-0.1	-0.1	0.3	1.7
20	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.0	0.0
20	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.6	0.0
21	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.0	0.0
21	0	ÌÝÐÎ° ÉÔØ	Z	-0.1	-0.1	0.3	1.7
21	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.0	0.0
22	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.0	0.0
22	0	ÌÝÐÎ° ÉÔØ	Z	-0.1	-0.1	0.3	1.7
22	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.9	0.0
23	0	ÌÝÐÎ° ÉÔØ	Z	-0.2	-0.2	0.7	1.2
24	0	ÌÝÐÎ° ÉÔØ	Z	-0.2	-0.2	0.7	1.2
25	0	ÌÝÐÎ° ÉÔØ	Z	-0.2	-0.2	0.7	1.2
26	0	ÌÝÐÎ° ÉÔØ	Z	-0.1	-0.1	0.3	1.7
27	0	ÌÝÐÎ° ÉÔØ	Z	-0.1	-0.1	0.3	1.7
28	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.3	0.0
29	0	ÌÝÐÎ° ÉÔØ	Z	-0.3	-0.3	1.0	2.1
30	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.7	0.0
31	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.1	0.0
32	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.1	0.0

33	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.2	0.0	1.3	0.0
34	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	1.1	0.0
35	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	1.1	0.0
36	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.2	0.0	1.3	0.0
37	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.1	0.0	0.3	0.0
38	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.6	-0.6	1.0	2.1
39	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.4	0.0	0.7	0.0
40	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.1	0.0	0.3	0.0
41	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.3	-0.3	1.0	2.1
41	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.3	-0.3	1.0	2.1
42	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.4	0.0	0.7	0.0
43	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.3	-0.3	1.0	2.1
43	0	$\frac{3}{4}\hat{u}^2\frac{1}{4}\hat{E}\hat{O}\hat{O}$	Z	-0.2	-0.2	0.0	0.0
44	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.2	0.0	0.7	0.0
45	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.7	0.0
46	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.7	0.0
47	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.3	-0.3	1.0	2.1
48	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.1	-0.1	0.3	1.7
49	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	1.0	0.0
49	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.1	-0.1	0.3	1.7
49	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.2	0.0	0.9	0.0
50	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.1	0.0	0.3	0.0
51	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.2	-0.2	0.7	1.2
52	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	1.0	0.0
52	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.2	-0.2	0.7	1.2

52	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.9	0.0
53	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.7	0.0
54	0	ÌÝÐÎ°ÉÔØ	Z	-0.1	-0.1	0.3	1.7
55	0	ÌÝÐÎ°ÉÔØ	Z	-0.2	-0.2	0.7	1.2
56	0	ÌÝÐÎ°ÉÔØ	Z	-0.2	-0.2	0.7	1.2
56	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.0	0.0
56	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.0	0.0
57	0	ÌÝÐÎ°ÉÔØ	Z	-0.1	-0.1	0.2	1.7
57	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.0	0.0
57	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.0	0.0
58	0	ÌÝÐÎ°ÉÔØ	Z	-0.6	-0.6	1.0	2.1
59	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.4	0.0
59	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.6	0.0
60	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.3	0.0
61	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.4	0.0
61	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.6	0.0
62	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.4	0.0	0.7	0.0
63	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
64	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.4	0.0
65	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.4	0.0
66	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
67	0	ÌÝÐÎ°ÉÔØ	Z	-0.3	-0.3	1.0	2.1
68	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.3	0.0

		ÉÔØ					
109	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.9	0.0
110	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.4	0.0
110	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.7	0.0
111	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.4	0.0
111	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.7	0.0
112	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.9	0.0
112	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
113	0	¾û² ¼° ÉÔØ	Z	-0.2	-0.2	0.0	0.0
113	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.3	0.0
114	0	¾û² ¼° ÉÔØ	Z	-0.2	-0.2	0.0	0.0
114	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.3	0.0
115	0	ÌÝÐÎ° ÉÔØ	Z	-0.3	-0.3	1.0	2.1
115	0	ÌÝÐÎ° ÉÔØ	Z	-0.3	-0.3	1.0	2.1
116	0	ÌÝÐÎ° ÉÔØ	Z	-0.3	-0.3	1.0	2.1
116	0	¾û² ¼° ÉÔØ	Z	-0.4	-0.4	0.0	0.0
118	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.7	0.0
119	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.0	0.0
119	0	ÌÝÐÎ° ÉÔØ	Z	-0.1	-0.1	0.3	1.7
119	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
120	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.9	0.0
120	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
121	0	¾û² ¼° ÉÔØ	Z	-0.2	-0.2	0.0	0.0
121	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.6	0.0
122	0	Èý½ÇÐÎ°	Z	-0.1	0.0	0.3	0.0

		ÉÔØ					
123	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.5	0.0
123	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.3	0.0
124	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.3	0.0
125	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.7	0.0
126	0	ÌÝÐÎ°ÉÔØ	Z	-0.2	-0.2	0.7	1.2
127	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.0	0.0
127	0	ÌÝÐÎ°ÉÔØ	Z	-0.2	-0.2	0.7	1.2
127	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
128	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.9	0.0
128	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
129	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.7	0.0
129	0	¾û²¼°ÉÔØ	Z	-0.1	-0.1	0.0	0.0
130	0	¾û²¼°ÉÔØ	Z	-0.2	-0.2	0.0	0.0
130	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.6	0.0
131	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.5	0.0
131	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.3	0.0
132	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.4	0.0	0.7	0.0
133	0	ÌÝÐÎ°ÉÔØ	Z	-0.3	-0.3	1.0	2.1
133	0	¾û²¼°ÉÔØ	Z	-0.2	-0.2	0.0	0.0
134	0	ÌÝÐÎ°ÉÔØ	Z	-0.3	-0.3	1.0	2.1
134	0	ÌÝÐÎ°ÉÔØ	Z	-0.3	-0.3	1.0	2.1
136	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.0	0.0
136	0	ÌÝÐÎ°ÉÔØ	Z	-0.1	-0.1	0.3	1.7
136	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0

137	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.1	0.0	0.3	0.0
138	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.1	0.0	0.3	0.0
139	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	1.0	0.0
139	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.2	-0.2	0.7	1.2
139	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.1	0.0	1.3	0.0
140	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.2	-0.2	0.7	1.2
141	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.2	0.0	0.7	0.0
142	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.4	0.0	0.7	0.0
143	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.2	-0.2	0.7	1.2
143	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	1.0	0.0
143	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.2	0.0	1.0	0.0
144	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.2	-0.2	0.7	1.2
145	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	1.0	0.0
145	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.1	-0.1	0.3	1.7
145	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.2	0.0	1.0	0.0
146	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.1	-0.1	0.3	1.7
147	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.9	0.0
148	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.9	0.0
149	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.1	-0.1	0.2	1.7
150	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.2	-0.2	0.7	1.2
151	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.1	-0.1	0.3	1.7
151	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	1.0	0.0
151	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.2	0.0	1.0	0.0
152	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.2	-0.2	0.7	1.2
152	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	1.0	0.0

152	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.2	0.0	1.0	0.0
153	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.6	0.0
153	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.4	0.0
154	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.6	0.0
154	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.4	0.0
155	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.6	-0.6	1.0	2.1
156	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.4	0.0
156	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.6	0.0
157	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.1	0.0	0.3	0.0
158	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.4	0.0
158	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.6	0.0
159	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.4	0.0	0.7	0.0
160	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.6	-0.6	1.0	2.1
161	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.1	0.0	0.3	0.0
162	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.4	0.0	0.7	0.0
163	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.7	0.0
164	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.7	0.0
165	0	$\hat{I}y\hat{D}\hat{I}^\circ\hat{E}\hat{O}\hat{O}$	Z	-0.3	-0.3	1.0	2.1
166	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.3	0.0
167	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.1	0.0	0.3	0.0
168	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$ $\hat{E}\hat{O}\hat{O}$	Z	-0.3	0.0	0.3	0.0
169	0	$\hat{E}y\frac{1}{2}\hat{C}\hat{D}\hat{I}^\circ$	Z	-0.2	0.0	0.7	0.0

		ÉÔØ					
170	0	ÏÝÐÎ°ÉÔØ	Z	-0.3	-0.3	1.0	2.1
171	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.3	0.0
172	0	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.7	0.0
175	0	¾Û²¼°ÉÔØ	Z	-0.2	-0.2	0.0	0.0
176	0	¾Û²¼°ÉÔØ	Z	-0.1	-0.1	0.0	0.0
212	0	ÏÝÐÎ°ÉÔØ	Z	-0.1	-0.1	0.3	1.7
213	0	ÏÝÐÎ°ÉÔØ	Z	-0.1	-0.1	0.3	1.7
222	0	¾Û²¼°ÉÔØ	Z	-0.0	-0.0	0.0	0.0
223	0	¾Û²¼°ÉÔØ	Z	-0.0	-0.0	0.0	0.0
224	0	¾Û²¼°ÉÔØ	Z	-0.1	-0.1	0.0	0.0
225	0	¾Û²¼°ÉÔØ	Z	-0.1	-0.1	0.0	0.0
226	0	¾Û²¼°ÉÔØ	Z	-0.4	-0.4	0.0	0.0
227	0	¾Û²¼°ÉÔØ	Z	-0.4	-0.4	0.0	0.0
228	0	¾Û²¼°ÉÔØ	Z	-0.0	-0.0	0.0	0.0
229	0	¾Û²¼°ÉÔØ	Z	-0.0	-0.0	0.0	0.0
230	0	¾Û²¼°ÉÔØ	Z	-0.3	-0.3	0.0	0.0
231	0	¾Û²¼°ÉÔØ	Z	-0.3	-0.3	0.0	0.0

μÚ 1 ' Ω¿öμ¥Øª°ÉÔØ±1

单元号	工况号	类型	方向	Q1	Q2	X1	X2
5	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.3	0.0
6	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.3	0.0
7	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.6	0.0
7	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.4	0.0
8	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.6	0.0
8	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.4	0.0
9	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.4	0.0
9	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.7	0.0
10	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.4	0.0

		ÉÔØ					
10	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.7	0.0
11	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.3	0.0
12	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.6	0.0
13	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.9	0.0
13	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
14	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.9	0.0
14	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
16	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.6	0.0
17	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	1.0	0.0
18	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.9	0.0
20	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	0.6	0.0
21	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	1.0	0.0
22	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.9	0.0
31	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	1.1	0.0
32	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	1.1	0.0
33	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.3	0.0
34	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	1.1	0.0
35	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	1.1	0.0
36	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	1.3	0.0
45	1	Èý½ÇÐÎ°	Z	-0.5	0.0	0.7	0.0

		ÉÔØ					
46	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.7	0.0
49	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.9	0.0
52	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.9	0.0
56	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	1.0	0.0
57	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	1.0	0.0
59	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.4	0.0
59	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.6	0.0
61	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.4	0.0
61	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.6	0.0
63	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
64	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.4	0.0
65	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.4	0.0
66	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
73	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.3	0.0
74	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.3	0.0
92	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	1.0	0.0
93	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	1.0	0.0
96	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.9	0.0
97	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.9	0.0
100	1	Èý½ÇÐÎ°	Z	-0.2	0.0	1.0	0.0

		ÉÔØ					
101	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	1.0	0.0
109	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
109	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.9	0.0
110	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.4	0.0
110	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.7	0.0
111	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.4	0.0
111	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.7	0.0
112	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.9	0.0
112	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
113	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.3	0.0
114	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.3	0.0
118	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.7	0.0
119	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.2	0.0	1.3	0.0
120	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	0.9	0.0
120	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.1	0.0	1.3	0.0
121	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.6	0.0
121	1	¾u² ¼° ÉÔØ	Z	-0.1	-0.1	0.0	0.0
123	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.5	0.0
123	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.3	0.0
125	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.3	0.0	0.7	0.0

127	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.2	0.0	1.3	0.0
128	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.1	0.0	0.9	0.0
128	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.1	0.0	1.3	0.0
130	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.3	0.0	0.6	0.0
130	1	$\frac{3}{4} \hat{I}^{\circ} \frac{1}{4} \hat{E} \hat{O} \emptyset$	Z	-0.1	-0.1	0.0	0.0
131	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.5	0.0	0.5	0.0
131	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.3	0.0	0.3	0.0
136	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.2	0.0	1.3	0.0
139	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.2	0.0	1.3	0.0
143	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.3	0.0	1.0	0.0
145	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.3	0.0	1.0	0.0
147	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.5	0.0	0.9	0.0
148	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.5	0.0	0.9	0.0
151	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.3	0.0	1.0	0.0
152	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.3	0.0	1.0	0.0
153	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.5	0.0	0.6	0.0
153	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.5	0.0	0.4	0.0
154	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.5	0.0	0.6	0.0
154	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.5	0.0	0.4	0.0
156	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$ $\hat{E} \hat{O} \emptyset$	Z	-0.5	0.0	0.4	0.0
156	1	$\hat{E}^{\circ} \hat{C} \hat{D} \hat{I}^{\circ}$	Z	-0.5	0.0	0.6	0.0

		ÉÔØ					
158	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.4	0.0
158	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.6	0.0
163	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.7	0.0
164	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.7	0.0
166	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.3	0.0
168	1	Èý½ÇÐÎ° ÉÔØ	Z	-0.5	0.0	0.3	0.0
222	1	¾û²¼°ÉÔØ	Z	-0.1	-0.1	0.0	0.0
223	1	¾û²¼°ÉÔØ	Z	-0.1	-0.1	0.0	0.0
226	1	¾û²¼°ÉÔØ	Z	-0.1	-0.1	0.0	0.0
227	1	¾û²¼°ÉÔØ	Z	-0.1	-0.1	0.0	0.0
228	1	¾û²¼°ÉÔØ	Z	-0.1	-0.1	0.0	0.0
229	1	¾û²¼°ÉÔØ	Z	-0.1	-0.1	0.0	0.0
230	1	¾û²¼°ÉÔØ	Z	-0.1	-0.1	0.0	0.0
231	1	¾û²¼°ÉÔØ	Z	-0.1	-0.1	0.0	0.0

μÚ 3 ' ΩΔöμΨθª°ÉÔØ±í

单元号	工况号	类型	方向	Q1	Q2	X1	X2
15	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
16	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
17	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
18	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
20	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
21	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
22	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
23	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
24	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
25	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
26	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
27	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
28	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
29	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0
30	3	¾û²¼°ÉÔØ	X	0.2	0.2	0.0	0.0

160	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
161	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
162	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
165	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
167	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
169	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
170	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
171	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
172	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
175	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
176	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
177	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
178	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
179	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
180	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
182	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
188	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
191	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
212	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
213	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
224	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
225	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
226	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
227	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
230	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
231	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
232	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
233	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
234	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0
235	3	¾û² ¼º ÉÔØ	X	0.2	0.2	0.0	0.0

μÚ 4 ¹ Ω¿öμ¥Øªº ÉÔØ±1

单元号	工况号	类型	方向	Q1	Q2	X1	X2
11	4	¾û² ¼º ÉÔØ	Z	0.2	0.2	0.0	0.0
12	4	¾û² ¼º ÉÔØ	Z	0.2	0.2	0.0	0.0
15	4	¾û² ¼º ÉÔØ	Z	0.2	0.2	0.0	0.0
16	4	¾û² ¼º ÉÔØ	Z	0.2	0.2	0.0	0.0
17	4	¾û² ¼º ÉÔØ	Z	0.2	0.2	0.0	0.0
18	4	¾û² ¼º ÉÔØ	Z	0.2	0.2	0.0	0.0

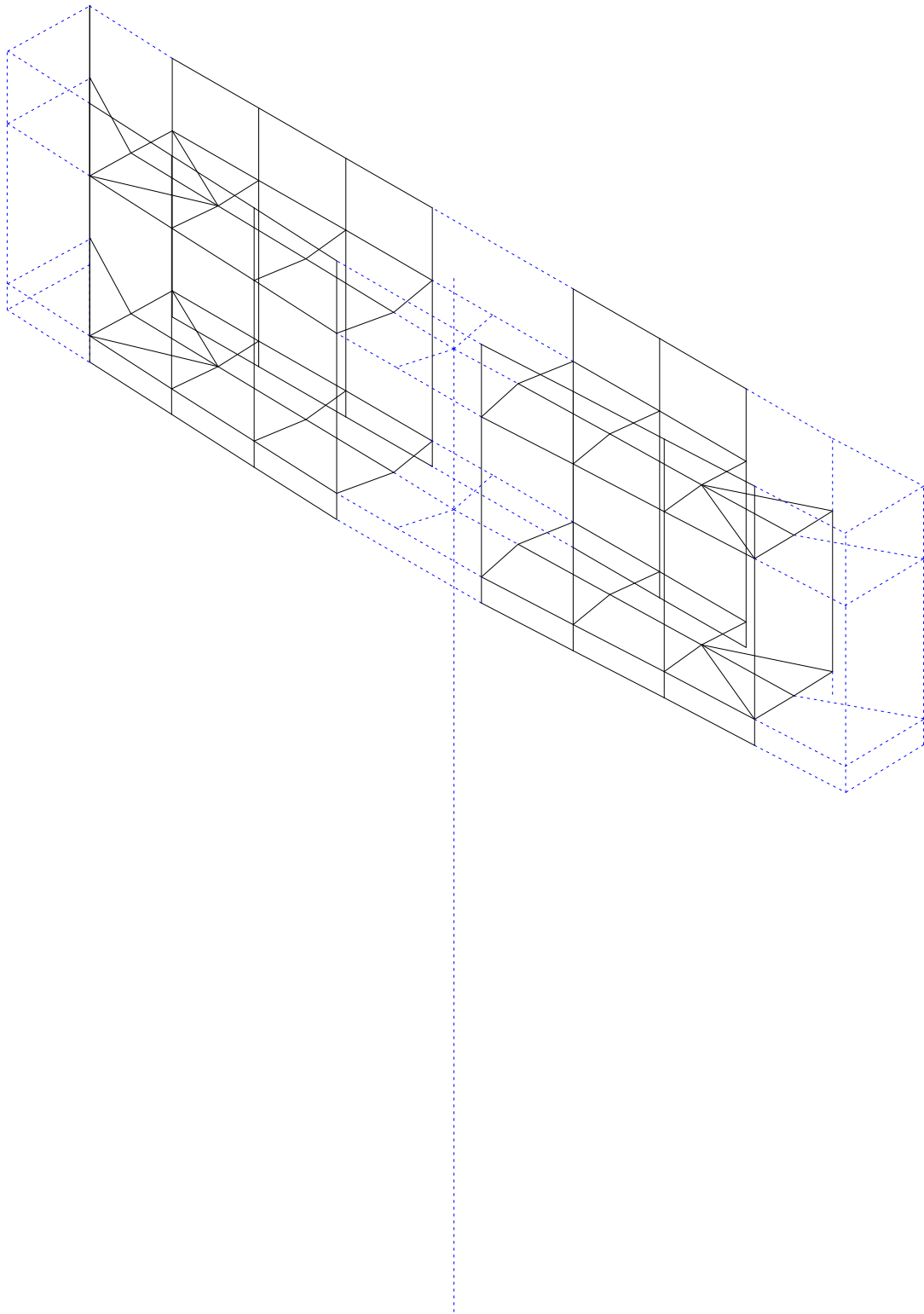
226	4	$\frac{3}{4}u^2 \frac{1}{4} \rho \hat{E} \hat{O} \hat{O}$	Z	0.2	0.2	0.0	0.0
227	4	$\frac{3}{4}u^2 \frac{1}{4} \rho \hat{E} \hat{O} \hat{O}$	Z	0.2	0.2	0.0	0.0
230	4	$\frac{3}{4}u^2 \frac{1}{4} \rho \hat{E} \hat{O} \hat{O}$	Z	0.2	0.2	0.0	0.0
231	4	$\frac{3}{4}u^2 \frac{1}{4} \rho \hat{E} \hat{O} \hat{O}$	Z	0.2	0.2	0.0	0.0
232	4	$\frac{3}{4}u^2 \frac{1}{4} \rho \hat{E} \hat{O} \hat{O}$	Z	0.2	0.2	0.0	0.0
233	4	$\frac{3}{4}u^2 \frac{1}{4} \rho \hat{E} \hat{O} \hat{O}$	Z	0.2	0.2	0.0	0.0
234	4	$\frac{3}{4}u^2 \frac{1}{4} \rho \hat{E} \hat{O} \hat{O}$	Z	0.2	0.2	0.0	0.0
235	4	$\frac{3}{4}u^2 \frac{1}{4} \rho \hat{E} \hat{O} \hat{O}$	Z	0.2	0.2	0.0	0.0

(1). 工况号: 0

*输入的面荷载:

序号	荷载类型	导荷方式	体形系数	面荷载值 (基本风压)
1	$\rho \hat{a} \hat{O} \hat{O}$	$\hat{E} \hat{K} \hat{I} \hat{O}, \hat{E} \hat{1} \hat{p}$	--	0.45

面荷载分布图:



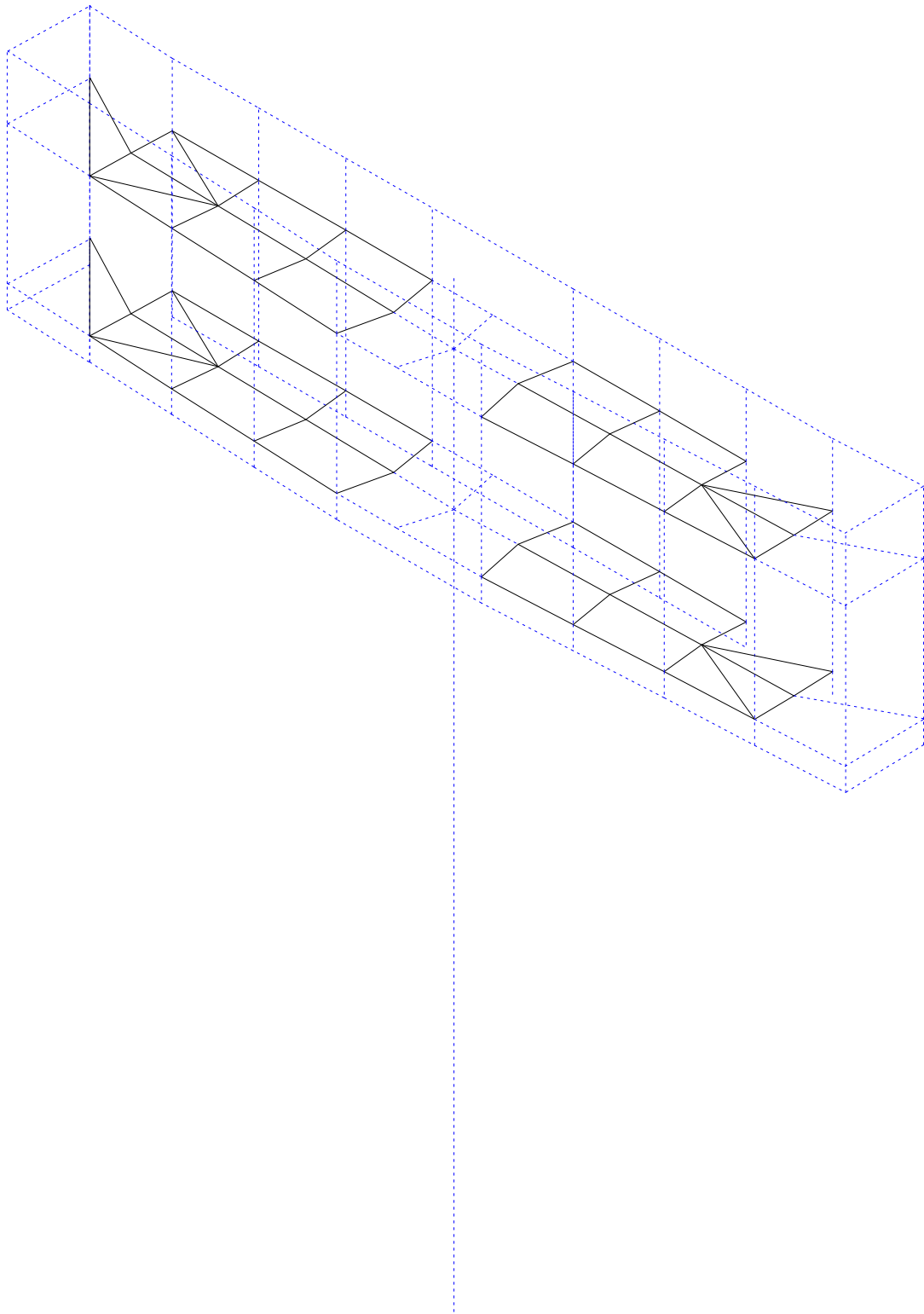
面荷载序号1分布图（实线表示荷载分配到的单元）

(2). 工况号: 1

*输入的面荷载:

序号	荷载类型	导荷方式	体形系数	面荷载值 (基本风压)
1	»î00	Ë«Ïò, È¼p	--	0.45

面荷载分布图:



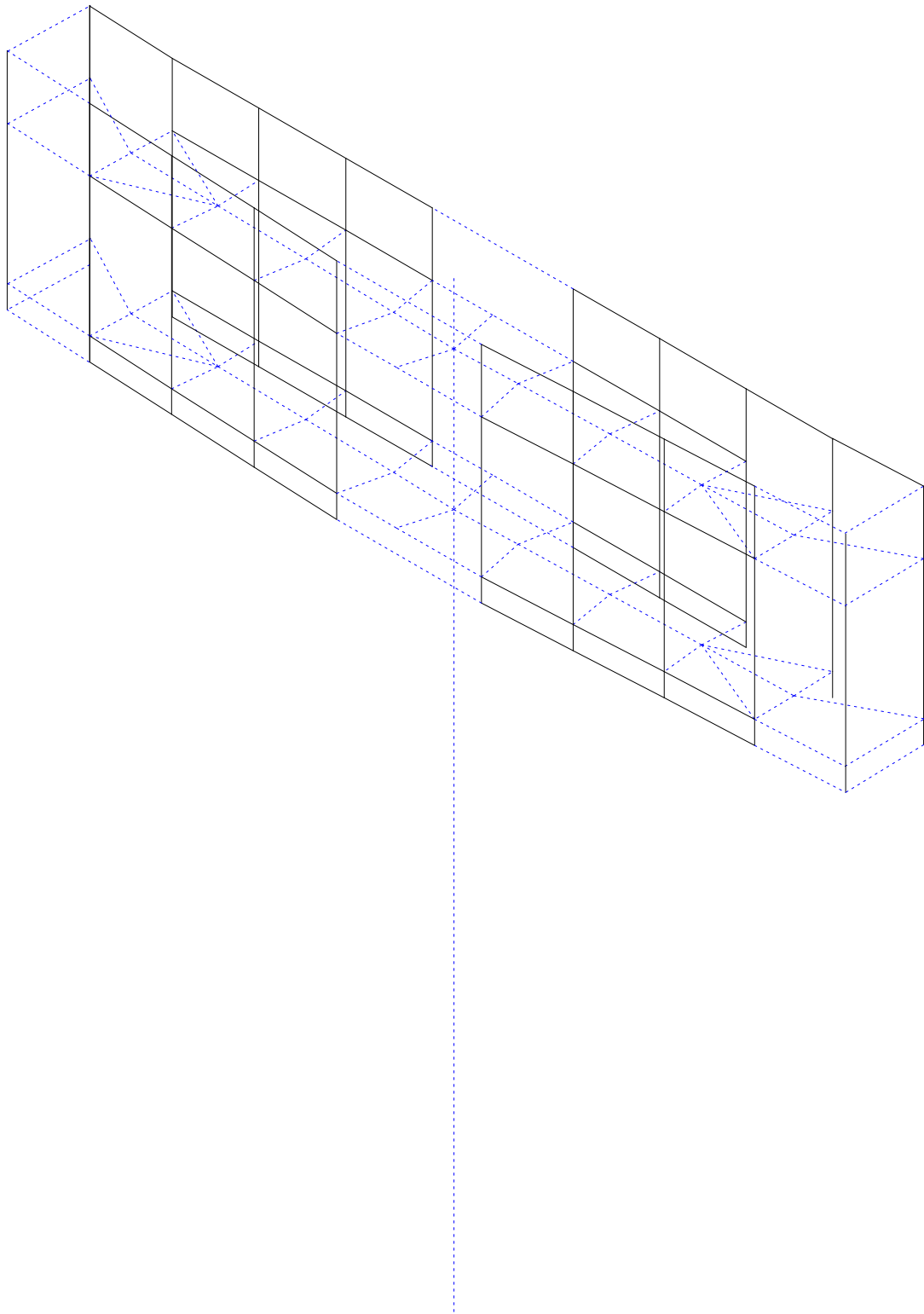
面荷载序号1分布图（实线表示荷载分配到的单元）

(3). 工况号: 3

*输入荷载库中的荷载:

序号	类型	方向	Q1 (kN)	Q2 (kN. m)	X1 (mm)	X2 (mm)
1	•Ö²¼°ÉÔØ	X	1.52	1.52	0.0	0.0

单元荷载分布图:



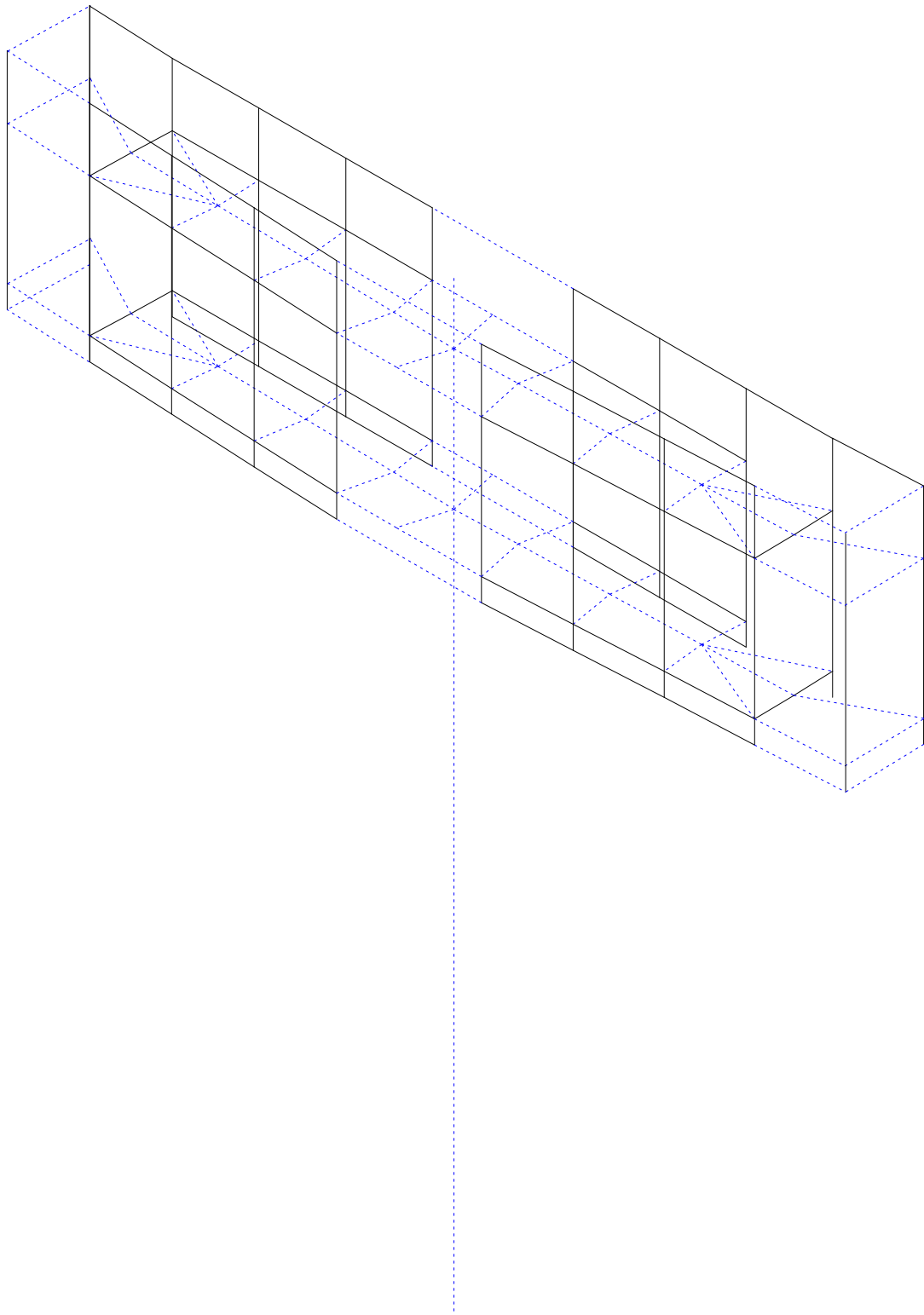
单元荷载序号1分布图（实线表示荷载作用的单元）

(4). 工况号: 4

*输入荷载库中的荷载:

序号	类型	方向	Q1 (kN)	Q2 (kN. m)	X1 (mm)	X2 (mm)
1	•Ö²¼°ÉÔØ	Z	1.52	1.52	0.0	0.0

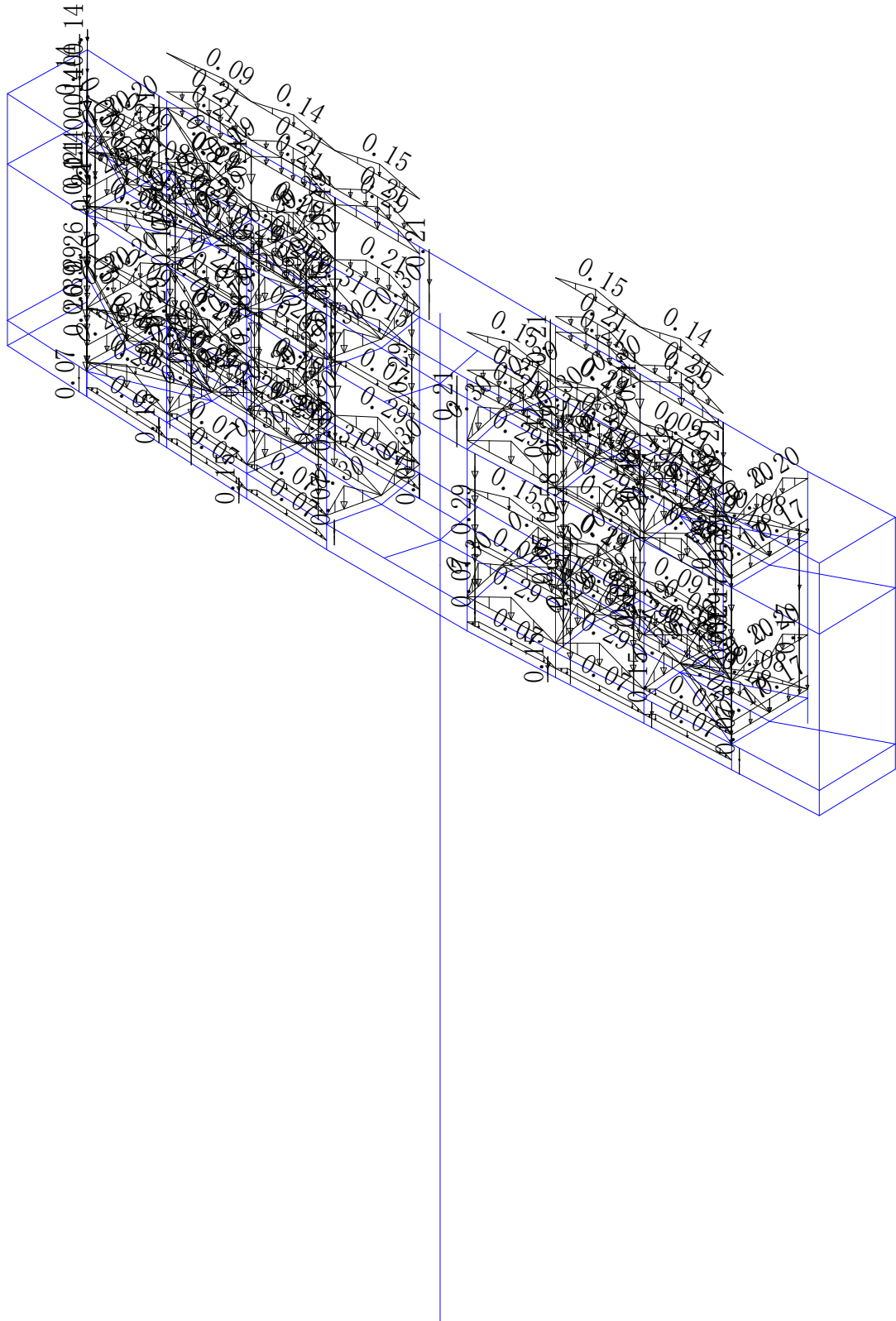
单元荷载分布图:



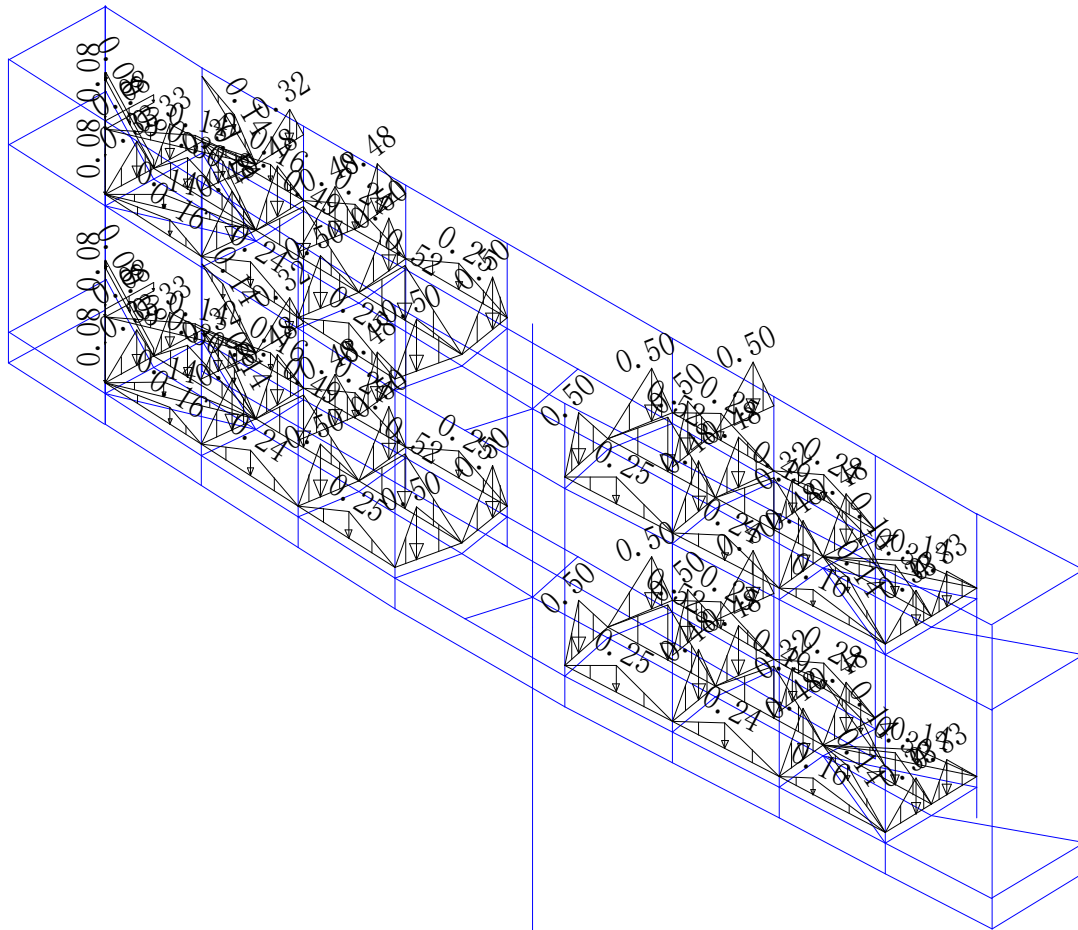
单元荷载序号1分布图（实线表示荷载作用的单元）

**以下为单元荷载图:

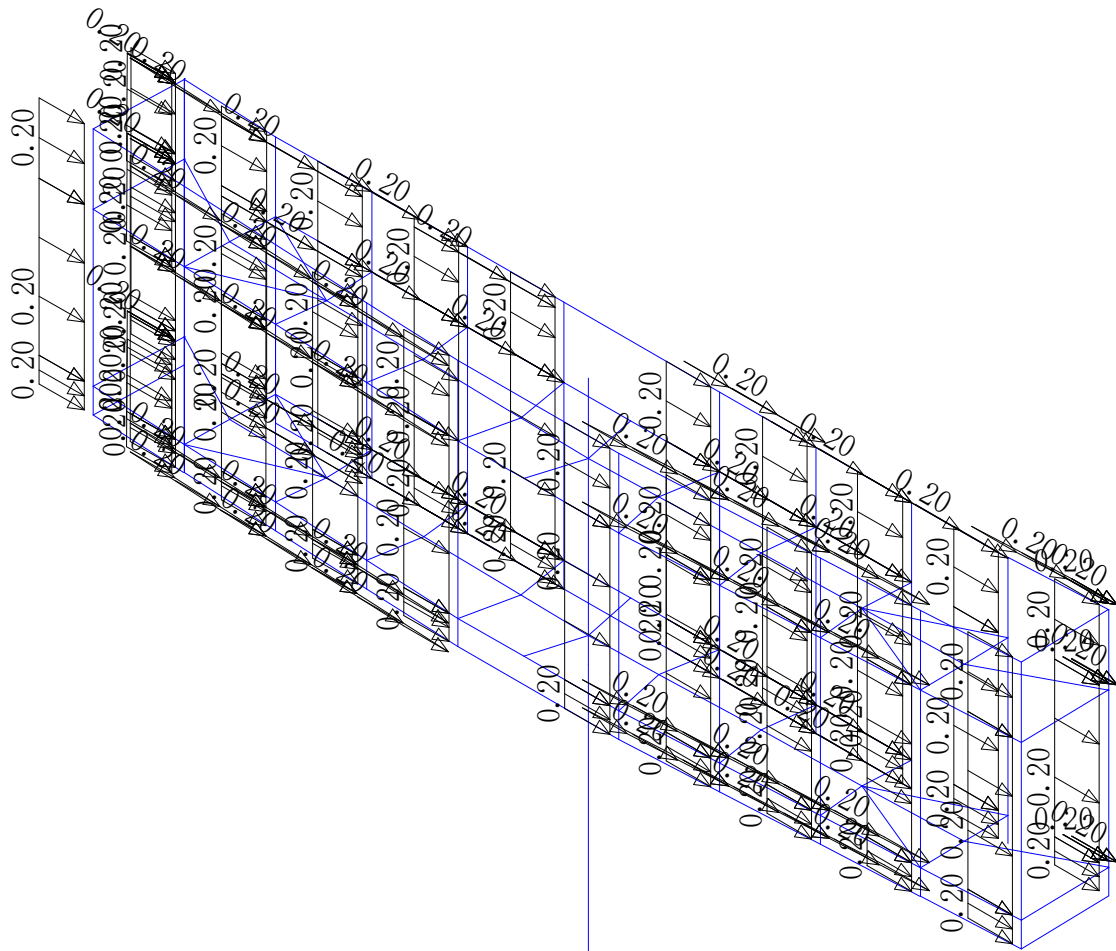
单位: 力(kN); 分布力(kN/m); 弯距(kN. m); 分布弯距(kN. m/m)



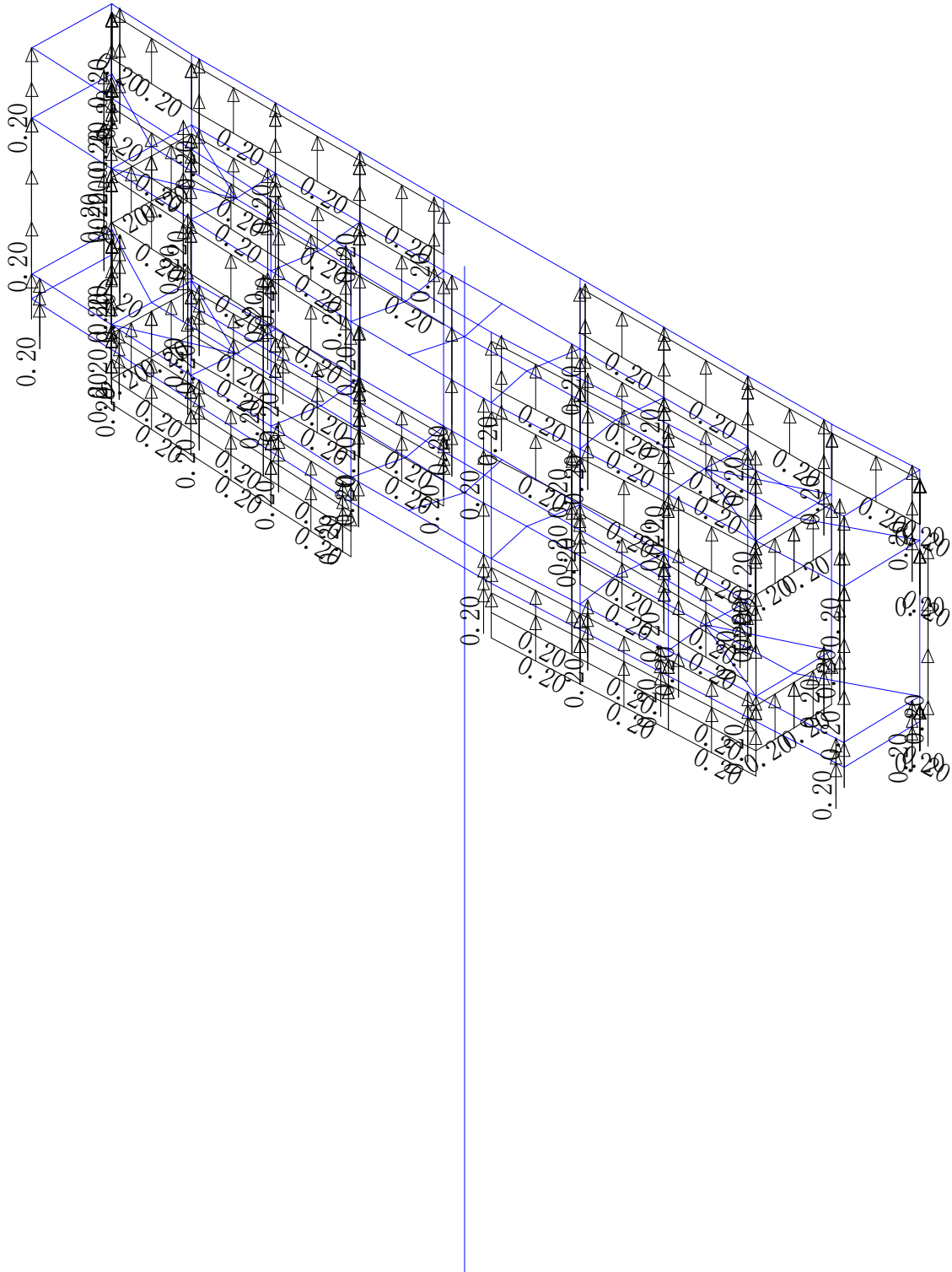
μύ 0 1 ΩιöμΨθ^a °É00%òÍ¼



μύ 1 ' Ωιöμψô°Éôø%οί¼



μύ 3 1 Ωζιöμψôª °ÉÔθ%δÍ¼



μύ 4 1 ΩζöμΨθ^a°Éθθ%δί¼

(三). 荷载组合

- (1) $1.20 \times \text{恒载} + 1.40 \times \text{活载}$
- (2) $1.20 \times \text{恒载} + 1.40 \times \text{活载}$
- (3) $1.20 \times \text{恒载} + 1.40 \times \text{活载}$
- (4) $1.20 \times \text{恒载} + 1.40 \times 0.90 \times \text{活载} + 1.40 \times 0.90 \times \text{活载}$
- (5) $1.20 \times \text{恒载} + 1.40 \times 0.90 \times \text{活载} + 1.40 \times 0.90 \times \text{活载}$
- (6) $1.20 \times \text{恒载}$

四、内力位移计算结果

(一). 内力

- 1. 工况内力
- 2. 组合内力
- 3. 最不利内力

× 10² (单位: N, Q(kN); M(kN.m); 位置(m))

单元号	名称	组合号	序号	位置	轴力 N	剪力 Q2	剪力 Q3	弯距 M2	弯距 M3
1	N×1'6	3	1	15.0	-205.0	0.0	-0.0	22.9	73.9
	M3×1'6	1	1	0.0	-379.2	0.0	-0.0	33.5	126.5
	N×1'6	1	1	0.0	-379.2	0.0	-0.0	33.5	126.5
	M3×1'6	2	1	0.0	-347.2	-56.4	0.0	30.5	-876.1
2	N×1'6	1	1	1.4	0.0	0.0	0.0	0.0	-0.0
	M3×1'6	2	1	1.4	0.0	-0.0	0.0	0.0	0.0
	N×1'6	3	1	0.0	-4.9	-0.0	0.0	-0.0	-0.0
	M3×1'6	3	1	0.0	-4.9	-0.0	0.0	-0.0	-0.0
3	N×1'6	3	1	0.5	-203.3	0.0	-0.0	22.9	73.9
	M3×1'6	1	1	0.0	-295.4	0.0	-0.0	33.5	126.5
	N×1'6	1	1	0.0	-295.4	0.0	-0.0	33.5	126.5

	$M3 \times \hat{D}_i$	2	1	0.0	-263.4	-56.4	0.0	30.5	-30.0
4	$N \times \hat{\sigma}$	3	1	0.0	-98.3	-5.4	-5.0	-2.4	18.0
	$M3 \times \hat{\sigma}$	1	1	3.1	-154.2	-9.4	-7.3	-26.3	59.7
	$N \times \hat{D}_i$	1	1	3.1	-154.2	-9.4	-7.3	-26.3	59.7
	$M3 \times \hat{D}_i$	2	1	3.1	-138.4	23.9	-6.7	-24.0	-37.3
5	$N \times \hat{\sigma}$	2	1	0.4	0.3	-9.1	-0.3	0.0	-3.0
	$M3 \times \hat{\sigma}$	1	1	1.1	-0.6	-12.5	-0.8	-0.5	5.1
	$N \times \hat{D}_i$	1	1	0.0	-0.6	-11.6	-0.8	0.4	-7.8
	$M3 \times \hat{D}_i$	1	1	0.0	-0.6	-11.6	-0.8	0.4	-7.8
6	$N \times \hat{\sigma}$	4	1	0.0	3.0	-9.7	2.1	-1.1	-6.6
	$M3 \times \hat{\sigma}$	4	1	1.1	3.0	-10.6	2.1	1.1	4.3
	$N \times \hat{D}_i$	3	1	1.0	1.7	-6.3	1.2	0.6	1.8
	$M3 \times \hat{D}_i$	4	1	0.0	3.0	-9.7	2.1	-1.1	-6.6
7	$N \times \hat{\sigma}$	4	1	0.2	2.0	-5.5	-0.9	0.3	-4.5
	$M3 \times \hat{\sigma}$	1	1	1.0	2.0	-7.2	-1.4	-0.7	0.9
	$N \times \hat{D}_i$	3	1	0.0	1.2	-3.5	-0.9	0.5	-3.5
	$M3 \times \hat{D}_i$	1	1	0.0	2.0	-5.9	-1.4	0.7	-5.6
8	$N \times \hat{\sigma}$	3	1	0.0	-1.1	-2.3	2.0	-1.0	-2.6
	$M3 \times \hat{\sigma}$	4	1	1.0	-1.8	-5.8	3.3	1.7	0.9
	$N \times \hat{D}_i$	4	1	0.8	-1.8	-5.7	3.3	1.1	-0.1

	$M3 \times \hat{D}_i$	4	1	0.0	-1.8	-4.5	3.3	-1.6	-4.3
9	$N \times \hat{\delta}$	3	1	0.1	-4.2	3.4	2.0	-0.8	0.2
	$M3 \times \hat{\delta}$	4	1	0.0	-6.6	5.8	3.1	-1.5	1.2
	$N \times \hat{D}_i$	4	1	0.0	-6.6	5.8	3.1	-1.5	1.2
	$M3 \times \hat{D}_i$	1	1	0.9	-6.4	4.8	2.9	1.4	-3.9
10	$N \times \hat{\delta}$	1	1	0.0	2.5	7.3	-1.5	0.7	1.0
	$M3 \times \hat{\delta}$	1	1	0.0	2.5	7.3	-1.5	0.7	1.0
	$N \times \hat{D}_i$	3	1	0.0	1.5	4.3	-1.0	0.5	0.4
	$M3 \times \hat{D}_i$	4	1	0.9	2.3	6.2	-1.1	-0.5	-5.4
11	$N \times \hat{\delta}$	3	1	0.0	-6.5	-1.4	1.4	-0.6	-0.9
	$M3 \times \hat{\delta}$	1	1	0.9	-9.6	-2.4	2.0	0.9	0.6
	$N \times \hat{D}_i$	4	1	0.0	-10. 3	-1.6	2.1	-0.9	-1.3
	$M3 \times \hat{D}_i$	4	1	0.0	-10. 3	-1.6	2.1	-0.9	-1.3
12	$N \times \hat{\delta}$	1	1	0.0	2.0	-1.1	-0.9	0.4	-1.4
	$M3 \times \hat{\delta}$	6	1	0.9	1.7	-1.7	-0.8	-0.3	0.0
	$N \times \hat{D}_i$	2	1	0.0	0.0	-1.1	-0.5	0.3	-1.2
	$M3 \times \hat{D}_i$	1	1	0.0	2.0	-1.1	-0.9	0.4	-1.4
13	$N \times \hat{\delta}$	4	1	0.0	33.8	0.7	0.2	-0.3	0.4
	$M3 \times \hat{\delta}$	1	1	0.0	32.1	0.7	0.2	-0.3	0.4
	$N \times \hat{D}_i$	3	1	0.2	21.7	0.4	0.1	-0.2	0.2

	$M3 \times \hat{D}_i$	1	1	1.5	32.1	0.0	0.2	0.0	-0.2
14	$N \times \hat{\delta}$	2	1	0.4	-8.9	0.5	-0.1	0.1	0.1
	$M3 \times \hat{\delta}$	1	1	0.0	-14.6	0.8	-0.1	0.2	0.4
	$N \times \hat{D}_i$	1	1	0.0	-14.6	0.8	-0.1	0.2	0.4
	$M3 \times \hat{D}_i$	2	1	2.2	-8.9	0.0	-0.1	-0.1	-0.3
15	$N \times \hat{\delta}$	3	1	0.0	-12.8	4.5	1.4	-2.3	3.8
	$M3 \times \hat{\delta}$	4	1	0.0	-18.0	6.7	2.2	-3.7	5.6
	$N \times \hat{D}_i$	4	1	1.9	-18.5	5.4	2.2	0.5	-6.1
	$M3 \times \hat{D}_i$	4	1	1.9	-18.5	5.4	2.2	0.5	-6.1
16	$N \times \hat{\delta}$	1	1	0.0	5.2	1.6	-0.1	0.2	1.1
	$M3 \times \hat{\delta}$	1	1	0.0	5.2	1.6	-0.1	0.2	1.1
	$N \times \hat{D}_i$	2	1	1.9	1.5	0.3	-0.1	-0.1	-0.6
	$M3 \times \hat{D}_i$	1	1	1.9	5.2	0.3	-0.1	-0.1	-0.7
17	$N \times \hat{\delta}$	3	1	0.5	-3.1	0.9	0.0	-0.0	0.3
	$M3 \times \hat{\delta}$	1	1	0.0	-4.2	1.6	0.1	-0.1	1.2
	$N \times \hat{D}_i$	4	1	1.9	-5.8	0.2	0.0	0.0	-0.6
	$M3 \times \hat{D}_i$	1	1	1.9	-4.2	0.2	0.1	0.1	-0.6
18	$N \times \hat{\delta}$	3	1	0.0	-9.3	0.8	0.1	-0.1	0.6
	$M3 \times \hat{\delta}$	1	1	0.0	-13.5	1.5	0.1	-0.1	1.0
	$N \times \hat{D}_i$	4	1	1.9	-13.8	0.0	0.1	0.1	-0.4

	$M3 \times \hat{D}_i$	1	1	1.9	-13.5	0.0	0.1	0.1	-0.4
19	$N \times \hat{\delta}$	3	1	0.0	-0.1	0.1	0.2	-0.2	-0.0
	$M3 \times \hat{\delta}$	3	1	1.8	-0.1	-0.2	0.2	0.3	0.1
	$N \times \hat{D}_i$	1	1	0.0	-0.2	0.1	0.4	-0.3	0.0
	$M3 \times \hat{D}_i$	4	1	0.9	-0.2	-0.0	0.3	0.1	-0.0
20	$N \times \hat{\delta}$	3	1	0.0	-10.2	0.6	0.0	-0.0	0.5
	$M3 \times \hat{\delta}$	1	1	0.0	-15.5	1.2	0.0	-0.0	0.9
	$N \times \hat{D}_i$	4	1	1.9	-16.5	0.2	0.0	-0.0	-0.5
	$M3 \times \hat{D}_i$	4	1	1.9	-16.5	0.2	0.0	-0.0	-0.5
21	$N \times \hat{\delta}$	4	1	0.0	8.1	1.3	-0.2	0.2	0.9
	$M3 \times \hat{\delta}$	1	1	0.0	8.0	1.3	-0.2	0.1	0.9
	$N \times \hat{D}_i$	3	1	0.0	5.9	0.7	-0.1	0.1	0.6
	$M3 \times \hat{D}_i$	6	1	1.9	7.6	0.2	-0.2	-0.2	-0.4
22	$N \times \hat{\delta}$	4	1	0.0	31.9	1.2	-0.2	0.2	0.8
	$M3 \times \hat{\delta}$	1	1	0.0	31.5	1.3	-0.2	0.1	0.9
	$N \times \hat{D}_i$	3	1	1.6	21.6	0.2	-0.1	-0.1	-0.2
	$M3 \times \hat{D}_i$	6	1	1.9	28.6	0.1	-0.2	-0.2	-0.3
23	$N \times \hat{\delta}$	4	1	0.0	45.2	6.2	-0.0	-0.1	6.5
	$M3 \times \hat{\delta}$	1	1	0.0	45.1	6.5	0.3	-0.5	6.7
	$N \times \hat{D}_i$	3	1	0.0	30.9	4.3	0.2	-0.3	4.5

	$M3 \times \hat{D}_i$	1	1	1.9	45.1	5.1	0.3	0.0	-4.4
24	$N \times \hat{\delta}$	4	1	0.0	33.1	6.1	0.4	-0.0	5.6
	$M3 \times \hat{\delta}$	1	1	0.0	33.0	6.3	0.6	-0.0	5.8
	$N \times \hat{D}_i$	3	1	0.0	22.8	4.2	0.4	-0.0	3.9
	$M3 \times \hat{D}_i$	1	1	1.9	33.0	4.9	0.6	1.1	-5.0
25	$N \times \hat{\delta}$	4	1	0.0	20.3	6.6	1.1	1.1	5.7
	$M3 \times \hat{\delta}$	1	1	0.0	20.3	6.8	1.1	1.3	5.8
	$N \times \hat{D}_i$	3	1	0.0	14.1	4.6	0.7	0.9	4.0
	$M3 \times \hat{D}_i$	1	1	1.9	20.3	5.4	1.1	3.3	-5.9
26	$N \times \hat{\delta}$	3	1	0.0	-32.0	-3.3	-1.0	2.5	-3.2
	$M3 \times \hat{\delta}$	1	1	1.9	-46.3	-6.0	-1.4	0.8	5.6
	$N \times \hat{D}_i$	1	1	0.0	-46.3	-4.7	-1.4	3.6	-4.7
	$M3 \times \hat{D}_i$	1	1	0.0	-46.3	-4.7	-1.4	3.6	-4.7
27	$N \times \hat{\delta}$	3	1	0.3	-50.7	-3.6	-0.8	0.8	-1.8
	$M3 \times \hat{\delta}$	1	1	1.9	-74.2	-6.3	-1.2	-0.7	6.6
	$N \times \hat{D}_i$	1	1	0.0	-74.2	-5.1	-1.2	1.6	-4.4
	$M3 \times \hat{D}_i$	1	1	0.0	-74.2	-5.1	-1.2	1.6	-4.4
28	$N \times \hat{\delta}$	1	1	0.0	7.1	-18.8	-5.3	2.4	-3.7
	$M3 \times \hat{\delta}$	1	1	0.5	6.8	-18.8	-5.3	-0.3	5.7
	$N \times \hat{D}_i$	3	1	0.5	4.8	-11.9	-3.6	-0.2	3.6

	$M3 \times \hat{D}_i$	1	1	0.0	7.1	-18.8	-5.3	2.4	-3.7
29	$N \times \hat{\delta}$	1	1	0.0	2.3	-1.1	-1.9	3.0	-1.6
	$M3 \times \hat{\delta}$	1	1	3.1	-0.1	-1.1	-1.9	-2.8	1.7
	$N \times \hat{D}_i$	2	1	3.1	-1.9	-0.6	-1.8	-2.9	1.5
	$M3 \times \hat{D}_i$	4	1	0.0	0.9	-1.5	-1.9	2.8	-1.9
30	$N \times \hat{\delta}$	3	1	1.4	-5.0	4.9	-1.9	-0.2	-3.8
	$M3 \times \hat{\delta}$	1	1	0.0	-8.0	7.6	-2.9	3.8	4.9
	$N \times \hat{D}_i$	1	1	0.0	-8.0	7.6	-2.9	3.8	4.9
	$M3 \times \hat{D}_i$	1	1	1.4	-7.0	7.6	-2.9	-0.2	-5.8
31	$N \times \hat{\delta}$	4	1	0.0	47.2	37.9	-0.2	-2.1	95.5
	$M3 \times \hat{\delta}$	4	1	0.0	47.2	37.9	-0.2	-2.1	95.5
	$N \times \hat{D}_i$	3	1	0.3	28.2	24.5	0.1	-1.6	55.5
	$M3 \times \hat{D}_i$	3	1	2.0	28.2	21.6	0.1	-1.6	17.1
32	$N \times \hat{\delta}$	4	1	0.0	37.6	20.4	-4.1	-3.9	33.7
	$M3 \times \hat{\delta}$	4	1	0.0	37.6	20.4	-4.1	-3.9	33.7
	$N \times \hat{D}_i$	3	1	1.7	22.2	11.6	-2.6	-6.8	2.5
	$M3 \times \hat{D}_i$	1	1	2.0	33.2	16.6	-3.8	-11.3	-4.3
33	$N \times \hat{\delta}$	2	1	0.2	-1.3	10.7	6.9	-12.0	7.2
	$M3 \times \hat{\delta}$	2	1	0.0	-1.3	11.0	6.9	-13.2	9.0
	$N \times \hat{D}_i$	1	1	0.0	-3.3	11.7	7.1	-13.0	6.8

	$M3 \times \hat{D}_i$	1	1	2.0	-3.3	8.1	7.1	1.3	-13.0
34	$N \times \hat{\delta}$	2	1	0.0	-10.6	35.3	0.2	0.0	89.3
	$M3 \times \hat{\delta}$	1	1	0.0	-23.3	41.3	0.5	-0.2	98.4
	$N \times \hat{D}_i$	1	1	0.0	-23.3	41.3	0.5	-0.2	98.4
	$M3 \times \hat{D}_i$	3	1	2.0	-15.5	24.2	0.3	0.5	15.3
35	$N \times \hat{\delta}$	2	1	0.0	-9.0	20.5	2.3	0.6	34.3
	$M3 \times \hat{\delta}$	4	1	0.0	-11.6	22.6	2.5	0.7	35.4
	$N \times \hat{D}_i$	1	1	0.0	-19.6	22.5	2.9	1.2	33.5
	$M3 \times \hat{D}_i$	1	1	2.0	-19.6	18.4	2.9	7.0	-7.5
36	$N \times \hat{\delta}$	2	1	0.0	-2.3	13.8	-1.5	5.3	10.8
	$M3 \times \hat{\delta}$	2	1	0.0	-2.3	13.8	-1.5	5.3	10.8
	$N \times \hat{D}_i$	1	1	0.2	-4.2	14.1	-2.9	7.0	5.7
	$M3 \times \hat{D}_i$	1	1	2.0	-4.2	10.7	-2.9	1.7	-17.0
37	$N \times \hat{\delta}$	2	1	0.0	1.4	-25.0	1.1	-0.3	-3.6
	$M3 \times \hat{\delta}$	1	1	0.5	0.9	-27.9	1.2	0.3	10.0
	$N \times \hat{D}_i$	5	1	0.5	0.5	-22.0	0.9	0.2	7.9
	$M3 \times \hat{D}_i$	1	1	0.0	1.2	-27.9	1.2	-0.3	-4.0
38	$N \times \hat{\delta}$	1	1	0.0	1.9	-1.7	-2.3	3.7	-2.4
	$M3 \times \hat{\delta}$	1	1	3.1	-1.3	-1.7	-2.3	-3.5	3.0
	$N \times \hat{D}_i$	2	1	3.1	-2.0	-1.2	-2.1	-3.5	2.6

	$M3 \times \hat{D}_i$	4	1	0.0	1.3	-2.2	-2.3	3.5	-2.7
39	$N \times \hat{\delta}$	5	1	1.4	-0.8	9.5	0.2	0.8	-8.0
	$M3 \times \hat{\delta}$	1	1	0.0	-2.4	12.1	0.3	0.7	6.7
	$N \times \hat{D}_i$	2	1	0.0	-2.5	10.1	0.2	0.6	5.6
	$M3 \times \hat{D}_i$	1	1	1.4	-1.2	12.1	0.3	1.0	-10.2
40	$N \times \hat{\delta}$	2	1	0.0	2.4	-25.7	4.8	-1.5	-3.4
	$M3 \times \hat{\delta}$	1	1	0.5	1.9	-27.8	4.9	0.9	10.2
	$N \times \hat{D}_i$	3	1	0.5	1.2	-19.0	3.3	0.6	7.0
	$M3 \times \hat{D}_i$	4	1	0.0	2.4	-27.8	5.2	-1.6	-3.7
41	$N \times \hat{\delta}$	4	1	3.1	1.9	2.5	-2.7	-3.5	-3.1
	$M3 \times \hat{\delta}$	1	1	0.0	-1.4	2.0	-2.7	4.8	3.5
	$N \times \hat{D}_i$	6	1	0.0	-1.4	1.9	-2.5	4.4	3.2
	$M3 \times \hat{D}_i$	4	1	3.1	1.9	2.5	-2.7	-3.5	-3.1
42	$N \times \hat{\delta}$	3	1	1.4	-1.2	8.7	0.1	0.7	-7.3
	$M3 \times \hat{\delta}$	1	1	0.0	-3.0	12.7	0.2	0.9	7.1
	$N \times \hat{D}_i$	2	1	0.0	-3.0	10.9	-0.1	1.0	6.0
	$M3 \times \hat{D}_i$	1	1	1.4	-1.9	12.7	0.2	1.1	-10.8
43	$N \times \hat{\delta}$	6	1	0.0	1.0	-1.9	1.7	-3.5	-2.6
	$M3 \times \hat{\delta}$	1	1	3.1	-2.2	-2.0	1.9	2.1	3.5
	$N \times \hat{D}_i$	4	1	3.1	-2.3	-1.7	1.9	2.0	3.4

	$M3 \times \hat{D}_i$	4	1	0.0	0.8	-2.5	1.9	-3.8	-3.1
44	$N \times \hat{\rho}$	1	1	1.4	1.0	11.2	-1.8	2.3	-9.2
	$M3 \times \hat{\rho}$	1	1	0.0	0.1	11.2	-1.8	4.8	6.4
	$N \times \hat{D}_i$	2	1	0.0	-0.2	9.6	-1.6	4.4	5.5
	$M3 \times \hat{D}_i$	1	1	1.4	1.0	11.2	-1.8	2.3	-9.2
45	$N \times \hat{\rho}$	2	1	0.0	2.2	8.8	0.6	-0.3	3.8
	$M3 \times \hat{\rho}$	1	1	0.0	1.4	11.7	1.6	-0.9	5.2
	$N \times \hat{D}_i$	3	1	0.0	1.0	7.6	1.1	-0.6	3.4
	$M3 \times \hat{D}_i$	1	1	1.1	1.4	10.9	1.6	0.9	-6.8
46	$N \times \hat{\rho}$	2	1	0.2	-0.0	10.7	-3.8	1.4	3.4
	$M3 \times \hat{\rho}$	4	1	0.0	-0.0	11.5	-4.0	2.2	5.5
	$N \times \hat{D}_i$	6	1	0.0	-0.4	9.2	-3.2	1.7	4.3
	$M3 \times \hat{D}_i$	4	1	1.1	-0.0	10.7	-4.0	-2.1	-6.3
47	$N \times \hat{\rho}$	1	1	3.1	1.6	1.0	2.7	4.4	-1.4
	$M3 \times \hat{\rho}$	1	1	0.0	-0.9	1.0	2.7	-4.0	1.7
	$N \times \hat{D}_i$	2	1	0.0	-2.6	0.5	2.6	-4.1	1.4
	$M3 \times \hat{D}_i$	4	1	3.1	0.1	1.4	2.8	4.3	-1.7
48	$N \times \hat{\rho}$	3	1	0.0	$-\frac{34}{3}$	4.4	0.4	-1.7	4.7
	$M3 \times \hat{\rho}$	1	1	0.0	$-\frac{50}{3}$	6.7	0.6	-2.6	7.0
	$N \times \hat{D}_i$	1	1	0.2	$-\frac{50}{3}$	6.6	0.6	-2.5	5.9

	$M3 \times \hat{i} \hat{D}_i$	1	1	1.9	-50.3	5.5	0.6	-1.4	-4.8
49	$N \times \hat{i}' \hat{o}$	4	1	0.0	34.0	1.3	0.2	-0.3	0.9
	$M3 \times \hat{i}' \hat{o}$	1	1	0.0	33.4	1.3	0.2	-0.2	0.9
	$N \times \hat{i} \hat{D}_i$	3	1	0.0	22.8	0.6	0.1	-0.2	0.5
	$M3 \times \hat{i} \hat{D}_i$	6	1	1.9	30.3	0.1	0.2	0.1	-0.4
50	$N \times \hat{i}' \hat{o}$	1	1	0.5	7.3	20.9	1.5	1.0	-4.1
	$M3 \times \hat{i}' \hat{o}$	1	1	0.0	7.0	20.9	1.5	0.2	6.3
	$N \times \hat{i} \hat{D}_i$	3	1	0.0	5.0	13.4	1.0	0.2	4.1
	$M3 \times \hat{i} \hat{D}_i$	4	1	0.5	7.3	20.7	1.8	1.2	-4.2
51	$N \times \hat{i}' \hat{o}$	4	1	0.0	24.6	6.5	0.0	0.7	6.8
	$M3 \times \hat{i}' \hat{o}$	1	1	0.0	24.1	6.8	-0.2	1.3	7.1
	$N \times \hat{i} \hat{D}_i$	3	1	0.2	16.3	4.5	-0.2	0.9	4.1
	$M3 \times \hat{i} \hat{D}_i$	1	1	1.9	24.1	5.4	-0.2	0.9	-4.7
52	$N \times \hat{i}' \hat{o}$	3	1	0.3	-9.9	0.8	-0.1	0.0	0.4
	$M3 \times \hat{i}' \hat{o}$	1	1	0.0	-14.8	1.5	-0.1	0.1	1.1
	$N \times \hat{i} \hat{D}_i$	1	1	0.0	-14.8	1.5	-0.1	0.1	1.1
	$M3 \times \hat{i} \hat{D}_i$	1	1	1.9	-14.8	0.1	-0.1	-0.1	-0.5
53	$N \times \hat{i}' \hat{o}$	3	1	1.4	-5.0	5.6	0.6	-0.2	-4.3
	$M3 \times \hat{i}' \hat{o}$	1	1	0.0	-8.0	8.6	0.9	-1.6	5.4
	$N \times \hat{i} \hat{D}_i$	1	1	0.0	-8.0	8.6	0.9	-1.6	5.4

	$M3 \times \hat{D}_i$	1	1	1.4	-7.0	8.6	0.9	-0.4	-6.6
54	$N \times \hat{\delta}$	3	1	1.6	-12.9	4.3	2.3	1.2	-3.0
	$M3 \times \hat{\delta}$	1	1	0.0	-18.6	7.2	3.4	-3.6	6.3
	$N \times \hat{D}_i$	4	1	1.9	-18.7	5.9	3.7	3.3	-6.3
	$M3 \times \hat{D}_i$	1	1	1.9	-18.6	5.9	3.4	2.9	-6.3
55	$N \times \hat{\delta}$	4	1	0.0	11.1	7.8	-1.1	1.4	6.5
	$M3 \times \hat{\delta}$	1	1	0.0	10.5	8.0	-1.5	1.7	6.8
	$N \times \hat{D}_i$	3	1	0.0	7.1	5.5	-1.0	1.1	4.6
	$M3 \times \hat{D}_i$	1	1	1.9	10.5	6.6	-1.5	-1.1	-7.4
56	$N \times \hat{\delta}$	3	1	0.3	-3.5	0.9	-0.1	0.1	0.5
	$M3 \times \hat{\delta}$	1	1	0.0	-5.3	1.7	-0.2	0.2	1.2
	$N \times \hat{D}_i$	4	1	1.9	-5.3	0.3	-0.1	-0.1	-0.6
	$M3 \times \hat{D}_i$	1	1	1.9	-5.3	0.3	-0.2	-0.2	-0.7
57	$N \times \hat{\delta}$	4	1	0.0	9.7	1.3	0.4	-0.4	0.9
	$M3 \times \hat{\delta}$	1	1	0.0	9.3	1.3	0.4	-0.4	0.9
	$N \times \hat{D}_i$	3	1	0.2	6.5	0.7	0.3	-0.2	0.5
	$M3 \times \hat{D}_i$	6	1	1.9	8.6	0.2	0.3	0.3	-0.4
58	$N \times \hat{\delta}$	1	1	3.1	0.8	1.6	1.0	1.7	-2.1
	$M3 \times \hat{\delta}$	1	1	0.0	-2.4	1.6	1.0	-1.4	2.8
	$N \times \hat{D}_i$	2	1	0.0	-3.1	1.1	1.0	-1.7	2.4

	$M3 \times \hat{i} \hat{D}_i$	4	1	3.1	0.2	2.0	1.1	1.6	-2.4
59	$N \times \hat{i}' \hat{o}$	4	1	0.0	2.6	7.7	-6.3	3.2	3.2
	$M3 \times \hat{i}' \hat{o}$	4	1	0.0	2.6	7.7	-6.3	3.2	3.2
	$N \times \hat{i} \hat{D}_i$	3	1	0.6	1.8	3.8	-3.8	-0.3	-0.8
	$M3 \times \hat{i} \hat{D}_i$	4	1	1.0	2.6	6.4	-6.3	-3.1	-3.9
60	$N \times \hat{i}' \hat{o}$	2	1	0.5	2.2	28.9	2.6	1.4	-4.3
	$M3 \times \hat{i}' \hat{o}$	1	1	0.0	1.7	31.7	2.8	0.1	11.2
	$N \times \hat{i} \hat{D}_i$	3	1	0.0	1.1	21.4	1.9	0.1	7.6
	$M3 \times \hat{i} \hat{D}_i$	4	1	0.5	2.1	31.6	2.8	1.5	-4.7
61	$N \times \hat{i}' \hat{o}$	2	1	0.0	-0.3	5.8	1.1	-0.6	1.8
	$M3 \times \hat{i}' \hat{o}$	1	1	0.0	-0.6	7.5	2.5	-1.2	2.5
	$N \times \hat{i} \hat{D}_i$	1	1	0.0	-0.6	7.5	2.5	-1.2	2.5
	$M3 \times \hat{i} \hat{D}_i$	1	1	1.0	-0.6	6.1	2.5	1.2	-4.3
62	$N \times \hat{i}' \hat{o}$	3	1	1.4	-1.8	9.2	0.8	0.0	-7.8
	$M3 \times \hat{i}' \hat{o}$	1	1	0.0	-3.7	13.6	1.2	-1.7	7.6
	$N \times \hat{i} \hat{D}_i$	4	1	0.0	-3.8	12.7	1.2	-1.6	7.0
	$M3 \times \hat{i} \hat{D}_i$	1	1	1.4	-2.6	13.6	1.2	0.0	-11.5
63	$N \times \hat{i}' \hat{o}$	3	1	0.2	-1.9	0.3	0.2	-0.1	0.1
	$M3 \times \hat{i}' \hat{o}$	1	1	0.0	-2.7	0.5	0.2	-0.3	0.3
	$N \times \hat{i} \hat{D}_i$	1	1	0.0	-2.7	0.5	0.2	-0.3	0.3

	$M3 \times \hat{1} \hat{D}_i$	4	1	1.6	-2.4	-0.0	0.3	0.2	-0.2
64	$N \times \hat{1}' \hat{o}$	1	1	0.0	1.4	-4.4	3.3	-1.6	-2.1
	$M3 \times \hat{1}' \hat{o}$	1	1	0.9	1.4	-5.1	3.3	1.5	2.4
	$N \times \hat{1} \hat{D}_i$	3	1	0.2	0.8	-3.6	2.2	-0.7	-1.2
	$M3 \times \hat{1} \hat{D}_i$	4	1	0.0	1.0	-4.3	2.1	-1.0	-2.2
65	$N \times \hat{1}' \hat{o}$	3	1	0.9	-2.0	-2.5	-5.0	-1.9	1.3
	$M3 \times \hat{1}' \hat{o}$	4	1	0.9	-3.5	-2.8	-8.2	-3.8	1.9
	$N \times \hat{1} \hat{D}_i$	4	1	0.0	-3.5	-2.1	-8.2	4.0	-0.5
	$M3 \times \hat{1} \hat{D}_i$	5	1	0.0	-2.4	-2.2	-5.9	2.8	-0.8
66	$N \times \hat{1}' \hat{o}$	2	1	0.0	4.2	0.3	-0.2	0.2	0.2
	$M3 \times \hat{1}' \hat{o}$	1	1	0.0	2.7	0.5	-0.2	0.2	0.2
	$N \times \hat{1} \hat{D}_i$	3	1	0.2	1.9	0.3	-0.1	0.1	0.1
	$M3 \times \hat{1} \hat{D}_i$	1	1	1.5	2.7	0.0	-0.2	-0.1	-0.2
67	$N \times \hat{1}' \hat{o}$	3	1	3.1	-0.1	1.4	-0.2	-0.5	-1.9
	$M3 \times \hat{1}' \hat{o}$	1	1	0.0	-2.8	2.0	-0.1	-0.0	3.5
	$N \times \hat{1} \hat{D}_i$	2	1	0.0	-2.9	1.5	-0.1	-0.2	3.1
	$M3 \times \hat{1} \hat{D}_i$	4	1	3.1	-0.4	2.4	-0.2	-0.7	-3.0
68	$N \times \hat{1}' \hat{o}$	3	1	0.0	-4.0	-12. 9	-2.3	1.4	-2.1
	$M3 \times \hat{1}' \hat{o}$	1	1	0.5	-5.9	-18. 6	-3.4	0.5	6.3
	$N \times \hat{1} \hat{D}_i$	1	1	0.5	-5.9	-18. 6	-3.4	0.5	6.3

	$M3 \times \hat{D}_i$	4	1	0.0	-5.6	$\frac{-18.8}{8}$	-3.7	2.3	-3.1
69	$N \times \hat{\delta}$	1	1	1.4	5.5	10.5	-1.5	0.3	-8.4
	$M3 \times \hat{\delta}$	1	1	0.0	4.6	10.5	-1.5	2.3	6.3
	$N \times \hat{D}_i$	3	1	0.0	3.5	7.1	-1.0	1.5	4.2
	$M3 \times \hat{D}_i$	1	1	1.4	5.5	10.5	-1.5	0.3	-8.4
70	$N \times \hat{\delta}$	3	1	0.0	-0.4	-0.5	0.4	0.0	-0.0
	$M3 \times \hat{\delta}$	3	1	0.0	-0.4	-0.5	0.4	0.0	-0.0
	$N \times \hat{D}_i$	4	1	0.0	-0.6	-0.8	0.6	0.0	-0.0
	$M3 \times \hat{D}_i$	4	1	0.0	-0.6	-0.8	0.6	0.0	-0.0
71	$N \times \hat{\delta}$	4	1	0.0	5.7	$\frac{-13.5}{5}$	-5.5	-1.0	-3.4
	$M3 \times \hat{\delta}$	3	1	0.0	3.8	-9.3	-3.7	-0.8	-2.2
	$N \times \hat{D}_i$	3	1	0.0	3.8	-9.3	-3.7	-0.7	-2.2
	$M3 \times \hat{D}_i$	4	1	0.0	5.7	$\frac{-13.5}{5}$	-5.5	-1.0	-3.4
72	$N \times \hat{\delta}$	3	1	3.1	-0.8	2.1	0.3	0.2	-3.3
	$M3 \times \hat{\delta}$	4	1	0.0	-4.1	2.8	0.6	-1.4	4.6
	$N \times \hat{D}_i$	4	1	0.0	-4.1	2.8	0.6	-1.4	4.6
	$M3 \times \hat{D}_i$	4	1	3.1	-1.7	3.6	0.6	0.4	-5.3
73	$N \times \hat{\delta}$	5	1	0.0	0.4	3.4	0.4	-0.1	2.0
	$M3 \times \hat{\delta}$	4	1	0.0	0.2	5.2	0.4	-0.1	3.0
	$N \times \hat{D}_i$	2	1	0.1	0.2	4.8	0.4	-0.1	2.5

	$M3 \times \hat{1} \hat{D}_i$	4	1	0.9	0.2	4.5	0.4	0.3	-1.3
74	$N \times \hat{1} \hat{\phi}$	6	1	0.0	-0.3	1.3	-0.4	0.1	0.5
	$M3 \times \hat{1} \hat{\phi}$	1	1	0.0	-0.4	1.4	-0.5	0.1	0.6
	$N \times \hat{1} \hat{D}_i$	2	1	0.0	-1.1	0.9	-0.5	0.2	0.2
	$M3 \times \hat{1} \hat{D}_i$	6	1	0.9	-0.3	0.7	-0.4	-0.3	-0.4
75	$N \times \hat{1} \hat{\phi}$	3	1	1.4	-0.5	-0.0	0.0	0.0	-0.5
	$M3 \times \hat{1} \hat{\phi}$	3	1	1.4	-0.5	-0.0	0.0	0.0	-0.5
	$N \times \hat{1} \hat{D}_i$	2	1	0.0	-1.9	-0.9	0.0	0.1	-2.1
	$M3 \times \hat{1} \hat{D}_i$	2	1	0.0	-1.9	-0.9	0.0	0.1	-2.1
76	$N \times \hat{1} \hat{\phi}$	3	1	0.5	-3.7	12.9	-0.7	-0.8	-2.2
	$M3 \times \hat{1} \hat{\phi}$	4	1	0.0	-5.4	18.6	-1.2	-0.6	6.1
	$N \times \hat{1} \hat{D}_i$	4	1	0.0	-5.4	18.6	-1.2	-0.6	6.1
	$M3 \times \hat{1} \hat{D}_i$	4	1	0.5	-5.1	18.7	-1.2	-1.3	-3.3
77	$N \times \hat{1} \hat{\phi}$	2	1	0.0	0.3	-0.1	0.0	-0.0	-0.0
	$M3 \times \hat{1} \hat{\phi}$	5	1	0.5	-0.0	-0.0	0.0	0.0	0.0
	$N \times \hat{1} \hat{D}_i$	3	1	0.5	-0.0	-0.0	0.0	0.0	0.0
	$M3 \times \hat{1} \hat{D}_i$	2	1	0.0	0.3	-0.1	0.0	-0.0	-0.0
78	$N \times \hat{1} \hat{\phi}$	2	1	0.0	-0.2	0.2	0.2	0.0	-0.0
	$M3 \times \hat{1} \hat{\phi}$	3	1	0.0	-0.2	0.2	0.2	0.0	-0.0
	$N \times \hat{1} \hat{D}_i$	1	1	0.0	-0.3	0.3	0.3	0.0	-0.0

	$M3 \times \hat{D}_i$	4	1	0.0	-0.2	0.2	0.2	0.0	-0.0
79	$N \times \hat{\delta}$	2	1	0.0	-0.2	1.5	-0.3	0.0	-0.0
	$M3 \times \hat{\delta}$	3	1	0.0	-0.2	-0.6	-0.5	-0.0	0.0
	$N \times \hat{D}_i$	1	1	0.0	-0.3	2.4	-0.7	-0.0	-0.0
	$M3 \times \hat{D}_i$	1	1	0.0	-0.3	2.4	-0.7	-0.0	-0.0
80	$N \times \hat{\delta}$	4	1	0.0	53.8	62.1	-3.6	3.9	175. 3
	$M3 \times \hat{\delta}$	4	1	0.0	53.8	62.1	-3.6	3.9	175. 3
	$N \times \hat{D}_i$	3	1	0.0	32.0	40.3	-2.1	1.9	114. 5
	$M3 \times \hat{D}_i$	3	1	1.4	32.0	38.2	-2.1	-1.1	60.2
81	$N \times \hat{\delta}$	2	1	0.1	-11. 0	55.5	2.2	-2.9	153. 0
	$M3 \times \hat{\delta}$	1	1	0.0	-25. 5	67.6	2.6	-4.2	184. 5
	$N \times \hat{D}_i$	1	1	0.0	-25. 5	67.6	2.6	-4.2	184. 5
	$M3 \times \hat{D}_i$	3	1	1.4	-17. 0	43.4	1.9	-0.4	63.1
82	$N \times \hat{\delta}$	3	1	0.3	-0.3	1.1	0.3	-0.1	0.7
	$M3 \times \hat{\delta}$	1	1	0.0	-0.5	1.5	0.5	-0.3	1.5
	$N \times \hat{D}_i$	4	1	0.3	-0.6	1.4	0.7	-0.2	1.1
	$M3 \times \hat{D}_i$	3	1	1.0	-0.3	0.9	0.3	0.2	0.0
83	$N \times \hat{\delta}$	3	1	0.1	-1.0	1.2	-1.1	0.6	1.1
	$M3 \times \hat{\delta}$	1	1	0.0	-1.5	1.6	-1.7	1.0	1.7
	$N \times \hat{D}_i$	4	1	0.0	-1.8	1.6	-2.1	1.3	1.6

	$M3 \times \hat{D}_i$	3	1	1.1	-1.0	0.9	-1.1	-0.6	0.0
84	$N \times \hat{\delta}$	1	1	0.0	0.9	1.6	0.9	-0.6	1.6
	$M3 \times \hat{\delta}$	4	1	0.0	0.5	1.6	0.3	-0.2	1.6
	$N \times \hat{D}_i$	2	1	0.2	0.4	1.5	0.2	-0.1	1.2
	$M3 \times \hat{D}_i$	3	1	1.1	0.6	0.9	0.6	0.3	0.0
85	$N \times \hat{\delta}$	1	1	0.6	0.1	1.4	-0.2	-0.0	0.6
	$M3 \times \hat{\delta}$	4	1	0.0	-0.2	1.6	0.2	-0.1	1.6
	$N \times \hat{D}_i$	2	1	0.1	-0.2	1.5	0.2	-0.1	1.3
	$M3 \times \hat{D}_i$	3	1	1.0	0.0	0.9	-0.1	-0.1	0.0
86	$N \times \hat{\delta}$	3	1	3.1	-0.4	0.0	-0.0	0.0	-0.0
	$M3 \times \hat{\delta}$	1	1	0.0	-2.5	0.0	-0.0	0.0	0.0
	$N \times \hat{D}_i$	2	1	0.0	-2.5	-1.3	-0.0	0.0	-2.8
	$M3 \times \hat{D}_i$	2	1	0.0	-2.5	-1.3	-0.0	0.0	-2.8
87	$N \times \hat{\delta}$	3	1	0.5	-1.3	-0.0	-0.0	0.0	0.0
	$M3 \times \hat{\delta}$	5	1	0.5	-1.4	-0.0	-0.0	0.0	0.0
	$N \times \hat{D}_i$	1	1	0.0	-2.8	-0.0	-0.0	0.0	-0.0
	$M3 \times \hat{D}_i$	2	1	0.0	-2.8	-1.4	-0.0	0.0	-3.5
88	$N \times \hat{\delta}$	3	1	1.4	-0.0	-0.0	0.0	0.0	0.0
	$M3 \times \hat{\delta}$	1	1	1.4	-0.0	-0.0	0.0	0.0	0.0
	$N \times \hat{D}_i$	1	1	0.0	-0.8	-0.0	0.0	-0.0	-0.0

	$M3 \times \hat{D}_i$	2	1	0.0	-0.8	-0.4	0.0	-0.0	-0.3
89	$N \times \hat{\delta}$	4	1	3.1	6.0	5.8	3.3	6.8	-8.4
	$M3 \times \hat{\delta}$	4	1	0.0	4.2	5.0	3.3	-3.4	8.2
	$N \times \hat{D}_i$	3	1	0.0	2.7	3.7	2.3	-2.5	5.7
	$M3 \times \hat{D}_i$	4	1	3.1	6.0	5.8	3.3	6.8	-8.4
90	$N \times \hat{\delta}$	2	1	0.5	5.2	1.5	0.0	7.9	1.9
	$M3 \times \hat{\delta}$	2	1	0.0	4.9	1.4	0.0	7.9	2.7
	$N \times \hat{D}_i$	3	1	0.0	3.5	0.0	0.0	5.4	-0.9
	$M3 \times \hat{D}_i$	3	1	0.5	3.6	0.0	0.0	5.4	-0.9
91	$N \times \hat{\delta}$	1	1	1.4	2.2	9.0	3.9	3.0	-3.9
	$M3 \times \hat{\delta}$	1	1	0.0	1.5	9.0	3.9	-2.5	8.7
	$N \times \hat{D}_i$	3	1	0.0	0.8	6.3	2.7	-2.0	6.0
	$M3 \times \hat{D}_i$	1	1	1.4	2.2	9.0	3.9	3.0	-3.9
92	$N \times \hat{\delta}$	4	1	0.0	15.7	-0.1	0.0	-0.1	-0.5
	$M3 \times \hat{\delta}$	1	1	1.9	14.3	-1.4	0.0	-0.0	1.0
	$N \times \hat{D}_i$	3	1	0.2	9.8	-0.3	0.0	-0.0	-0.3
	$M3 \times \hat{D}_i$	1	1	0.0	14.3	-0.1	0.0	-0.1	-0.5
93	$N \times \hat{\delta}$	2	1	0.0	-3.7	-0.3	-0.0	0.0	-0.6
	$M3 \times \hat{\delta}$	1	1	1.9	-8.1	-1.7	-0.1	-0.0	1.2
	$N \times \hat{D}_i$	1	1	0.0	-8.1	-0.3	-0.1	0.1	-0.6

	$M3 \times \hat{D}_i$	4	1	0.0	-4.7	-0.3	-0.0	0.0	-0.7
94	$N \times \hat{\delta}$	1	1	0.0	18.7	-4.4	-0.1	1.4	-4.5
	$M3 \times \hat{\delta}$	4	1	1.9	18.1	-6.0	0.0	1.2	5.5
	$N \times \hat{D}_i$	3	1	0.0	12.6	-3.0	-0.1	0.9	-3.0
	$M3 \times \hat{D}_i$	4	1	0.0	18.5	-4.6	0.0	1.1	-4.7
95	$N \times \hat{\delta}$	3	1	0.0	-24.3	-3.2	0.2	-1.5	-3.1
	$M3 \times \hat{\delta}$	1	1	1.9	-35.6	-5.9	0.2	-1.7	5.6
	$N \times \hat{D}_i$	1	1	0.0	-35.6	-4.7	0.2	-2.2	-4.7
	$M3 \times \hat{D}_i$	1	1	0.0	-35.6	-4.7	0.2	-2.2	-4.7
96	$N \times \hat{\delta}$	3	1	0.3	-13.7	-19.4	-1.1	3.1	-2.0
	$M3 \times \hat{\delta}$	1	1	2.0	-19.4	-33.0	-1.6	1.8	48.0
	$N \times \hat{D}_i$	2	1	0.0	-34.0	-25.7	-1.5	4.2	-12.3
	$M3 \times \hat{D}_i$	4	1	0.0	-33.8	-28.4	-1.6	4.6	-14.9
97	$N \times \hat{\delta}$	1	1	0.0	42.3	-26.1	1.8	-5.7	-11.3
	$M3 \times \hat{\delta}$	1	1	2.0	42.3	-30.1	1.8	-2.1	44.9
	$N \times \hat{D}_i$	2	1	0.0	23.7	-23.3	1.4	-5.2	-9.1
	$M3 \times \hat{D}_i$	4	1	0.0	28.5	-25.7	1.6	-5.6	-11.6
98	$N \times \hat{\delta}$	3	1	0.0	-37.3	-3.3	0.3	-0.8	-3.2
	$M3 \times \hat{\delta}$	1	1	1.9	-54.8	-6.1	0.4	-0.3	5.8
	$N \times \hat{D}_i$	1	1	0.0	-54.8	-4.8	0.4	-1.1	-4.7

	$M3 \times \hat{D}_i$	1	1	0.0	-54.8	-4.8	0.4	-1.1	-4.7
99	$N \times \hat{\delta}$	1	1	0.0	35.9	-5.0	-0.8	1.2	-5.1
	$M3 \times \hat{\delta}$	4	1	1.9	35.2	-6.5	-1.0	-0.7	6.0
	$N \times \hat{D}_i$	3	1	0.0	24.5	-3.4	-0.5	0.9	-3.4
	$M3 \times \hat{D}_i$	4	1	0.0	35.7	-5.1	-1.0	1.3	-5.2
100	$N \times \hat{\delta}$	4	1	0.0	14.9	-0.2	0.1	-0.1	-0.5
	$M3 \times \hat{\delta}$	1	1	1.9	14.1	-1.4	0.1	0.1	1.0
	$N \times \hat{D}_i$	3	1	0.0	9.6	-0.3	0.1	-0.1	-0.4
	$M3 \times \hat{D}_i$	4	1	0.0	14.9	-0.2	0.1	-0.1	-0.5
101	$N \times \hat{\delta}$	2	1	0.0	-3.4	-0.4	-0.0	0.0	-0.7
	$M3 \times \hat{\delta}$	1	1	1.9	-7.5	-1.7	0.0	0.0	1.3
	$N \times \hat{D}_i$	1	1	0.5	-7.5	-0.5	0.0	0.0	-0.5
	$M3 \times \hat{D}_i$	4	1	0.0	-4.3	-0.3	-0.0	0.0	-0.7
102	$N \times \hat{\delta}$	2	1	0.0	-0.2	1.7	0.3	-0.0	-0.0
	$M3 \times \hat{\delta}$	3	1	0.0	-0.2	-0.4	0.5	-0.0	-0.0
	$N \times \hat{D}_i$	1	1	0.0	-0.3	2.5	0.7	-0.0	-0.0
	$M3 \times \hat{D}_i$	1	1	0.0	-0.3	2.5	0.7	-0.0	-0.0
103	$N \times \hat{\delta}$	2	1	0.0	-3.4	-1.1	-1.1	0.8	-10.1
	$M3 \times \hat{\delta}$	3	1	0.0	-3.5	1.1	-0.3	-1.1	-9.5
	$N \times \hat{D}_i$	1	1	0.0	-5.0	-1.5	-0.4	-1.7	-13.2

	$M3 \times \hat{D}_i$	1	1	0.0	-5.0	-1.5	-0.4	-1.7	-13.2
104	$N \times \hat{\delta}$	2	1	2.7	-10.9	1.3	-3.2	-3.8	-2.9
	$M3 \times \hat{\delta}$	4	1	0.0	-13.4	2.9	-3.9	5.9	2.7
	$N \times \hat{D}_i$	1	1	0.2	-17.9	2.5	-3.5	5.8	1.9
	$M3 \times \hat{D}_i$	4	1	2.7	-12.9	1.4	-3.4	-3.9	-3.0
105	$N \times \hat{\delta}$	2	1	0.2	-3.8	4.3	-1.3	1.4	-4.6
	$M3 \times \hat{\delta}$	3	1	0.0	-4.0	4.4	-0.3	1.5	-3.6
	$N \times \hat{D}_i$	1	1	0.0	-5.7	4.8	-0.4	2.3	-6.4
	$M3 \times \hat{D}_i$	1	1	2.1	-5.7	1.6	-0.4	1.4	-13.1
106	$N \times \hat{\delta}$	2	1	0.0	-0.3	-1.2	0.0	-0.1	-0.0
	$M3 \times \hat{\delta}$	3	1	0.0	-0.3	-2.6	0.2	-0.1	0.0
	$N \times \hat{D}_i$	1	1	0.0	-0.4	-0.7	0.3	-0.1	-0.0
	$M3 \times \hat{D}_i$	6	1	0.0	-0.4	-1.3	0.3	-0.1	-0.0
107	$N \times \hat{\delta}$	1	1	0.0	3.7	4.8	-3.6	-2.3	-1.8
	$M3 \times \hat{\delta}$	3	1	0.0	2.6	3.9	-2.5	-1.6	-1.2
	$N \times \hat{D}_i$	3	1	0.0	2.6	3.9	-2.5	-1.6	-1.2
	$M3 \times \hat{D}_i$	1	1	0.0	3.7	4.8	-3.6	-2.3	-1.8
108	$N \times \hat{\delta}$	1	1	0.0	3.7	3.3	-9.1	10.8	2.1
	$M3 \times \hat{\delta}$	1	1	0.0	3.7	3.3	-9.1	10.8	2.1
	$N \times \hat{D}_i$	3	1	0.0	2.6	2.2	-6.3	7.5	1.3

	$M3 \times \hat{D}_i$	1	1	1.8	3.7	2.3	-9.1	-5.5	-2.9
109	$N \times \hat{\delta}$	3	1	0.0	-3.1	0.5	0.0	-0.0	0.2
	$M3 \times \hat{\delta}$	1	1	0.0	-4.4	0.8	0.1	-0.1	0.4
	$N \times \hat{D}_i$	2	1	0.5	-10.8	0.4	0.0	-0.0	0.0
	$M3 \times \hat{D}_i$	2	1	2.2	-10.8	0.0	0.0	0.0	-0.3
110	$N \times \hat{\delta}$	1	1	0.0	2.2	7.3	0.7	-0.3	3.4
	$M3 \times \hat{\delta}$	1	1	0.0	2.2	7.3	0.7	-0.3	3.4
	$N \times \hat{D}_i$	3	1	0.1	1.6	4.3	0.5	-0.2	1.7
	$M3 \times \hat{D}_i$	1	1	0.9	2.2	6.2	0.7	0.3	-3.0
111	$N \times \hat{\delta}$	2	1	0.0	-0.9	4.3	-0.6	0.3	1.5
	$M3 \times \hat{\delta}$	1	1	0.0	-1.3	5.0	0.0	-0.0	1.7
	$N \times \hat{D}_i$	1	1	0.0	-1.3	5.0	0.0	-0.0	1.7
	$M3 \times \hat{D}_i$	1	1	0.9	-1.3	4.0	0.0	0.0	-2.6
112	$N \times \hat{\delta}$	1	1	0.0	14.2	0.7	-0.0	0.0	0.4
	$M3 \times \hat{\delta}$	1	1	0.0	14.2	0.7	-0.0	0.0	0.4
	$N \times \hat{D}_i$	2	1	0.0	8.1	0.5	-0.0	0.0	0.2
	$M3 \times \hat{D}_i$	1	1	1.5	14.2	-0.0	-0.0	0.0	-0.2
113	$N \times \hat{\delta}$	2	1	0.2	6.4	-3.0	-0.7	0.2	0.0
	$M3 \times \hat{\delta}$	4	1	0.9	6.3	-3.7	-0.6	-0.2	2.4
	$N \times \hat{D}_i$	3	1	0.0	2.5	-2.4	-0.2	0.1	-0.6

	$M3 \times \hat{D}_i$	2	1	0.0	6.4	-2.8	-0.7	0.3	-0.6
114	$N \times \hat{\delta}$	2	1	0.1	-5.7	0.3	0.7	-0.3	1.1
	$M3 \times \hat{\delta}$	1	1	0.9	-8.8	-0.6	1.2	0.5	1.4
	$N \times \hat{D}_i$	1	1	0.0	-8.8	0.2	1.2	-0.6	1.2
	$M3 \times \hat{D}_i$	3	1	0.0	-6.0	-0.5	0.8	-0.4	0.5
	$N \times \hat{\delta}$	1	1	3.1	1.6	-3.3	-0.7	-0.3	4.6
115	$M3 \times \hat{\delta}$	1	1	3.1	1.6	-3.3	-0.7	-0.3	4.6
	$N \times \hat{D}_i$	6	1	0.0	-1.6	-2.9	-0.6	1.7	-5.0
	$M3 \times \hat{D}_i$	1	1	0.0	-1.6	-3.3	-0.7	1.8	-5.5
	$N \times \hat{\delta}$	6	1	3.1	1.5	-3.1	1.7	2.8	4.3
116	$M3 \times \hat{\delta}$	1	1	3.1	1.5	-3.4	1.9	3.1	4.8
	$N \times \hat{D}_i$	4	1	0.0	-2.4	-3.6	1.7	-2.4	-5.7
	$M3 \times \hat{D}_i$	1	1	0.0	-2.4	-3.4	1.9	-2.9	-5.7
	$N \times \hat{\delta}$	2	1	0.0	-0.3	1.1	-0.3	0.0	-0.0
117	$M3 \times \hat{\delta}$	2	1	0.0	-0.3	1.1	-0.3	0.0	-0.0
	$N \times \hat{D}_i$	1	1	0.0	-0.5	0.8	-0.5	-0.0	-0.0
	$M3 \times \hat{D}_i$	1	1	0.0	-0.5	0.8	-0.5	-0.0	-0.0
	$N \times \hat{\delta}$	1	1	0.0	10.7	-8.8	1.7	-8.5	-21.6
118	$M3 \times \hat{\delta}$	6	1	2.0	9.8	-11.7	1.5	-4.7	1.6
	$N \times \hat{D}_i$	2	1	0.0	3.6	-8.4	0.7	-6.0	-19.1

	$M3 \times \hat{D}_i$	4	1	0.0	5.0	-8.7	0.9	-6.9	-21.6
119	$N \times \hat{\delta}$	2	1	0.0	-2.3	-0.2	0.0	-0.1	-0.4
	$M3 \times \hat{\delta}$	1	1	1.9	-4.4	-1.3	0.0	-0.0	0.9
	$N \times \hat{D}_i$	1	1	0.0	-4.4	-0.2	0.0	-0.1	-0.5
	$M3 \times \hat{D}_i$	1	1	0.0	-4.4	-0.2	0.0	-0.1	-0.5
120	$N \times \hat{\delta}$	1	1	0.0	17.6	0.2	-0.0	-0.0	-0.1
	$M3 \times \hat{\delta}$	1	1	2.2	17.6	-0.7	-0.0	-0.1	0.4
	$N \times \hat{D}_i$	3	1	0.0	12.2	0.1	-0.0	-0.0	-0.1
	$M3 \times \hat{D}_i$	1	1	0.7	17.6	-0.0	-0.0	-0.0	-0.2
121	$N \times \hat{\delta}$	1	1	0.0	1.3	-2.3	-0.6	0.3	-2.4
	$M3 \times \hat{\delta}$	2	1	0.9	-0.4	-3.1	-0.4	-0.2	0.3
	$N \times \hat{D}_i$	2	1	0.1	-0.4	-2.5	-0.4	0.1	-1.9
	$M3 \times \hat{D}_i$	1	1	0.0	1.3	-2.3	-0.6	0.3	-2.4
122	$N \times \hat{\delta}$	2	1	0.5	-0.9	-13.8	-2.4	-3.8	1.1
	$M3 \times \hat{\delta}$	1	1	0.5	-1.4	-16.1	-6.3	-4.8	1.3
	$N \times \hat{D}_i$	1	1	0.0	-1.7	-16.1	-6.3	-1.7	-6.8
	$M3 \times \hat{D}_i$	1	1	0.0	-1.7	-16.1	-6.3	-1.7	-6.8
123	$N \times \hat{\delta}$	1	1	0.0	1.1	-3.8	-1.6	0.7	-3.5
	$M3 \times \hat{\delta}$	4	1	0.9	0.9	-4.9	-1.3	-0.6	0.7
	$N \times \hat{D}_i$	2	1	0.0	0.8	-3.8	-1.1	0.5	-3.2

	$M3 \times \hat{D}_i$	1	1	0.0	1.1	-3.8	-1.6	0.7	-3.5
124	$N \times \hat{\delta}$	2	1	0.5	1.3	-21. 3	-0.5	-0.9	2.0
	$M3 \times \hat{\delta}$	1	1	0.5	1.1	-23. 4	-0.7	-1.0	2.1
	$N \times \hat{D}_i$	5	1	0.0	0.4	-18. 4	-0.5	-0.5	-7.5
	$M3 \times \hat{D}_i$	1	1	0.0	0.8	-23. 4	-0.7	-0.7	-9.6
125	$N \times \hat{\delta}$	3	1	0.0	-5.0	-7.8	0.6	1.9	-16. 6
	$M3 \times \hat{\delta}$	6	1	2.0	-6.5	-14. 6	0.7	4.2	3.3
	$N \times \hat{D}_i$	4	1	0.3	-11. 0	-12. 1	0.5	3.3	-22. 0
	$M3 \times \hat{D}_i$	4	1	0.0	-11. 0	-11. 6	0.5	3.1	-26. 0
126	$N \times \hat{\delta}$	4	1	0.0	23.9	-5.4	-4.2	9.2	-5.9
	$M3 \times \hat{\delta}$	4	1	1.9	23.4	-6.7	-4.2	1.1	5.8
	$N \times \hat{D}_i$	3	1	0.2	16.4	-3.6	-2.7	5.6	-3.2
	$M3 \times \hat{D}_i$	4	1	0.0	23.9	-5.4	-4.2	9.2	-5.9
127	$N \times \hat{\delta}$	2	1	0.0	5.2	-0.4	0.0	0.1	-0.7
	$M3 \times \hat{\delta}$	1	1	1.9	0.4	-1.7	0.0	0.1	1.2
	$N \times \hat{D}_i$	3	1	0.0	0.3	-0.4	0.0	0.0	-0.6
	$M3 \times \hat{D}_i$	1	1	0.0	0.4	-0.4	0.0	0.0	-0.7
128	$N \times \hat{\delta}$	3	1	0.0	-5.6	0.0	0.0	0.0	-0.2
	$M3 \times \hat{\delta}$	1	1	2.2	-8.0	-0.8	0.0	0.0	0.5
	$N \times \hat{D}_i$	4	1	0.0	-12. 3	0.1	0.0	0.0	-0.3

	$M3 \times \hat{D}_i$	2	1	0.0	-12. 2	-0.1	0.0	0.0	-0.4
129	$N \times \hat{\delta}$	5	1	1.4	-1.5	-8.4	-0.6	3.9	7.3
	$M3 \times \hat{\delta}$	4	1	1.4	-1.9	-11. 0	-0.6	5.3	9.5
	$N \times \hat{D}_i$	2	1	0.0	-3.2	-10. 6	-0.6	5.7	-5.8
	$M3 \times \hat{D}_i$	4	1	0.0	-3.1	-11. 3	-0.6	6.2	-6.2
130	$N \times \hat{\delta}$	2	1	0.0	0.8	-5.7	0.4	-0.2	-3.6
	$M3 \times \hat{\delta}$	1	1	0.9	0.1	-6.8	0.2	0.1	1.8
	$N \times \hat{D}_i$	5	1	0.1	-0.0	-4.1	0.1	-0.0	-2.5
	$M3 \times \hat{D}_i$	4	1	0.0	0.8	-5.8	0.4	-0.2	-3.8
131	$N \times \hat{\delta}$	3	1	0.0	-1.7	-3.4	0.6	-0.3	-3.5
	$M3 \times \hat{\delta}$	4	1	0.9	-2.5	-6.7	1.2	0.6	0.4
	$N \times \hat{D}_i$	4	1	0.0	-2.5	-5.7	1.2	-0.6	-5.5
	$M3 \times \hat{D}_i$	1	1	0.0	-2.4	-5.7	0.8	-0.4	-5.5
132	$N \times \hat{\delta}$	3	1	1.4	-1.0	-8.2	-1.7	0.4	7.2
	$M3 \times \hat{\delta}$	4	1	1.4	-1.6	-12. 5	-2.6	0.7	11.0
	$N \times \hat{D}_i$	2	1	0.0	-2.8	-11. 9	-2.4	4.0	-6.3
	$M3 \times \hat{D}_i$	4	1	0.0	-2.8	-12. 8	-2.6	4.3	-6.7
133	$N \times \hat{\delta}$	3	1	3.1	-0.1	-2.1	0.1	0.0	3.0
	$M3 \times \hat{\delta}$	1	1	3.1	-0.4	-3.2	0.3	0.2	4.5
	$N \times \hat{D}_i$	1	1	0.0	-3.5	-3.2	0.3	-0.7	-5.3

	$M3 \times \hat{D}_i$	4	1	0.0	-3.4	-3.4	0.3	-0.7	-5.3
134	$N \times \hat{\rho}$	3	1	3.1	-0.3	-2.0	0.2	-0.0	2.9
	$M3 \times \hat{\rho}$	1	1	3.1	-0.5	-3.1	0.4	0.2	4.4
	$N \times \hat{D}_i$	4	1	0.0	-3.8	-3.4	0.5	-1.2	-5.2
	$M3 \times \hat{D}_i$	4	1	0.0	-3.8	-3.4	0.5	-1.2	-5.2
135	$N \times \hat{\rho}$	2	1	0.0	-1.8	-6.1	0.4	-3.2	-17.9
	$M3 \times \hat{\rho}$	3	1	0.0	-2.0	-2.1	0.5	-2.6	-13.3
	$N \times \hat{D}_i$	1	1	0.0	-2.9	-6.3	0.7	-3.7	-18.9
	$M3 \times \hat{D}_i$	4	1	0.0	-2.1	-6.8	0.5	-3.5	-19.2
136	$N \times \hat{\rho}$	2	1	0.0	-1.5	-0.2	-0.1	0.0	-0.4
	$M3 \times \hat{\rho}$	1	1	1.9	-5.3	-1.2	-0.1	-0.1	0.8
	$N \times \hat{D}_i$	1	1	0.0	-5.3	-0.1	-0.1	0.1	-0.4
	$M3 \times \hat{D}_i$	1	1	0.0	-5.3	-0.1	-0.1	0.1	-0.4
137	$N \times \hat{\rho}$	3	1	0.5	-3.0	-8.4	-1.5	-1.3	0.8
	$M3 \times \hat{\rho}$	6	1	0.5	-3.8	-11.2	-2.1	-1.8	1.0
	$N \times \hat{D}_i$	1	1	0.0	-4.5	-12.1	-2.2	-0.8	-5.1
	$M3 \times \hat{D}_i$	1	1	0.0	-4.5	-12.1	-2.2	-0.8	-5.1
138	$N \times \hat{\rho}$	6	1	0.5	1.5	-21.4	2.3	1.4	2.1
	$M3 \times \hat{\rho}$	1	1	0.5	1.4	-23.6	2.5	1.5	2.3
	$N \times \hat{D}_i$	5	1	0.0	0.6	-18.4	1.9	0.2	-7.4

	$M3 \times \hat{D}_i$	1	1	0.0	1.1	-23.6	2.5	0.3	-9.4
139	$N \times \hat{\delta}$	2	1	0.0	4.8	-0.3	0.1	-0.1	-0.6
	$M3 \times \hat{\delta}$	4	1	1.9	3.8	-1.6	0.1	0.1	1.1
	$N \times \hat{D}_i$	1	1	0.0	-0.4	-0.3	0.1	-0.1	-0.6
	$M3 \times \hat{D}_i$	4	1	0.0	4.3	-0.3	0.1	-0.1	-0.7
140	$N \times \hat{\delta}$	1	1	1.8	7.8	-6.3	1.4	1.7	4.2
	$M3 \times \hat{\delta}$	4	1	1.9	7.3	-6.6	1.4	1.8	5.4
	$N \times \hat{D}_i$	3	1	0.0	5.3	-3.5	1.0	-0.5	-4.0
	$M3 \times \hat{D}_i$	4	1	0.0	7.7	-5.2	1.4	-0.9	-6.0
141	$N \times \hat{\delta}$	4	1	1.4	4.2	-8.2	-1.4	0.4	7.1
	$M3 \times \hat{\delta}$	4	1	1.4	4.2	-8.2	-1.4	0.4	7.1
	$N \times \hat{D}_i$	3	1	0.0	2.4	-5.3	-1.0	1.6	-2.9
	$M3 \times \hat{D}_i$	4	1	0.0	3.2	-8.6	-1.4	2.3	-4.7
142	$N \times \hat{\delta}$	3	1	1.4	-1.4	-7.3	1.0	0.2	6.5
	$M3 \times \hat{\delta}$	4	1	1.4	-2.1	-11.3	1.4	0.2	10.0
	$N \times \hat{D}_i$	2	1	0.0	-3.2	-10.8	1.2	-1.5	-5.6
	$M3 \times \hat{D}_i$	4	1	0.0	-3.2	-11.6	1.4	-1.7	-6.0
143	$N \times \hat{\delta}$	3	1	0.0	-10.6	-0.2	-0.1	0.1	-0.3
	$M3 \times \hat{\delta}$	4	1	1.9	-14.1	-1.4	-0.1	-0.1	1.0
	$N \times \hat{D}_i$	1	1	0.0	-15.8	0.0	-0.2	0.2	-0.4

	$M3 \times \hat{1} \hat{D}_i$	4	1	0.0	-13.6	-0.0	-0.1	0.1	-0.4
144	$N \times \hat{1} \hat{\sigma}$	1	1	0.3	28.5	-4.4	-0.9	0.7	-2.1
	$M3 \times \hat{1} \hat{\sigma}$	4	1	1.9	27.9	-5.8	-0.7	-0.5	6.2
	$N \times \hat{1} \hat{D}_i$	3	1	0.2	19.2	-2.9	-0.6	0.6	-1.8
	$M3 \times \hat{1} \hat{D}_i$	4	1	0.0	28.4	-4.4	-0.7	0.9	-3.7
145	$N \times \hat{1} \hat{\sigma}$	4	1	0.0	36.6	0.0	0.1	-0.1	-0.3
	$M3 \times \hat{1} \hat{\sigma}$	1	1	1.9	36.3	-1.2	0.1	0.1	0.8
	$N \times \hat{1} \hat{D}_i$	3	1	0.0	24.5	-0.2	0.1	-0.1	-0.3
	$M3 \times \hat{1} \hat{D}_i$	2	1	0.0	33.5	-0.1	0.1	-0.1	-0.3
146	$N \times \hat{1} \hat{\sigma}$	3	1	0.0	-40.6	-3.1	1.0	-1.1	-2.5
	$M3 \times \hat{1} \hat{\sigma}$	1	1	1.9	-60.0	-5.8	1.5	1.3	6.1
	$N \times \hat{1} \hat{D}_i$	1	1	0.0	-60.0	-4.5	1.5	-1.6	-3.8
	$M3 \times \hat{1} \hat{D}_i$	1	1	0.0	-60.0	-4.5	1.5	-1.6	-3.8
147	$N \times \hat{1} \hat{\sigma}$	3	1	0.0	-13.7	-28.6	-0.8	1.7	23.3
	$M3 \times \hat{1} \hat{\sigma}$	1	1	2.0	-19.4	-48.6	-1.2	0.1	127.0
	$N \times \hat{1} \hat{D}_i$	2	1	0.0	-35.2	-39.9	-1.3	1.7	29.7
	$M3 \times \hat{1} \hat{D}_i$	3	1	0.0	-13.7	-28.6	-0.8	1.7	23.3
148	$N \times \hat{1} \hat{\sigma}$	1	1	0.0	43.1	-45.4	0.3	-2.9	34.5
	$M3 \times \hat{1} \hat{\sigma}$	1	1	2.0	43.1	-49.5	0.3	-2.2	129.5
	$N \times \hat{1} \hat{D}_i$	2	1	0.5	23.7	-39.2	-0.0	-3.1	50.8

	$M3 \times \hat{D}_i$	3	1	0.0	29.7	-29.0	0.2	-1.9	23.8
149	$N \times \hat{\delta}$	3	1	0.2	-54.2	-3.3	0.0	-0.4	-2.2
	$M3 \times \hat{\delta}$	1	1	1.9	-80.1	-6.0	-0.0	-0.7	6.5
	$N \times \hat{D}_i$	1	1	0.0	-80.1	-4.8	-0.0	-0.6	-4.0
	$M3 \times \hat{D}_i$	4	1	0.0	-77.0	-4.8	-0.3	-0.7	-4.0
150	$N \times \hat{\delta}$	1	1	0.0	47.1	-4.8	0.3	-0.2	-4.0
	$M3 \times \hat{\delta}$	4	1	1.9	46.3	-6.4	0.0	-0.3	6.8
	$N \times \hat{D}_i$	3	1	0.0	32.1	-3.3	0.1	-0.1	-2.7
	$M3 \times \hat{D}_i$	4	1	0.0	46.8	-5.0	0.1	-0.4	-4.2
151	$N \times \hat{\delta}$	4	1	0.0	35.8	-0.0	0.0	-0.1	-0.3
	$M3 \times \hat{\delta}$	4	1	1.9	35.3	-1.2	0.0	-0.0	0.9
	$N \times \hat{D}_i$	3	1	0.0	24.0	-0.2	0.0	-0.1	-0.3
	$M3 \times \hat{D}_i$	2	1	0.0	32.8	-0.1	0.0	-0.1	-0.3
152	$N \times \hat{\delta}$	3	1	0.5	-10.4	-0.3	-0.0	0.0	-0.3
	$M3 \times \hat{\delta}$	1	1	1.9	-15.4	-1.5	-0.1	-0.0	1.0
	$N \times \hat{D}_i$	1	1	0.0	-15.4	-0.1	-0.1	0.1	-0.5
	$M3 \times \hat{D}_i$	4	1	0.0	-13.5	-0.1	-0.1	0.1	-0.5
153	$N \times \hat{\delta}$	4	1	0.0	0.7	5.6	-0.1	0.1	1.1
	$M3 \times \hat{\delta}$	4	1	0.0	0.7	5.6	-0.1	0.1	1.1
	$N \times \hat{D}_i$	3	1	0.0	0.4	2.9	0.3	-0.2	0.3

	$M3 \times \hat{D}_i$	4	1	1.0	0.7	4.3	-0.1	-0.1	-3.9
154	$N \times \hat{\delta}$	2	1	0.2	0.0	6.3	-0.7	0.2	1.2
	$M3 \times \hat{\delta}$	1	1	0.0	-0.2	8.2	-0.2	0.1	3.1
	$N \times \hat{D}_i$	1	1	0.0	-0.2	8.2	-0.2	0.1	3.1
	$M3 \times \hat{D}_i$	1	1	1.0	-0.2	6.9	-0.2	-0.1	-4.5
155	$N \times \hat{\delta}$	2	1	3.1	1.2	-2.0	-1.7	-2.3	3.2
	$M3 \times \hat{\delta}$	1	1	3.1	0.5	-2.8	-2.0	-2.5	4.0
	$N \times \hat{D}_i$	1	1	0.0	-2.7	-2.8	-2.0	3.7	-4.7
	$M3 \times \hat{D}_i$	1	1	0.0	-2.7	-2.8	-2.0	3.7	-4.7
156	$N \times \hat{\delta}$	3	1	0.0	-0.9	-3.3	-0.9	0.4	-3.0
	$M3 \times \hat{\delta}$	1	1	1.0	-1.5	-7.1	-1.3	-0.7	1.5
	$N \times \hat{D}_i$	1	1	0.3	-1.5	-6.1	-1.3	0.2	-3.0
	$M3 \times \hat{D}_i$	1	1	0.0	-1.5	-5.7	-1.3	0.6	-4.9
157	$N \times \hat{\delta}$	6	1	0.5	1.6	-22. 6	0.7	-0.2	2.6
	$M3 \times \hat{\delta}$	1	1	0.5	1.6	-25. 3	0.8	-0.2	2.9
	$N \times \hat{D}_i$	3	1	0.0	0.7	-16. 9	0.6	-0.4	-6.5
	$M3 \times \hat{D}_i$	4	1	0.0	1.2	-25. 3	0.7	-0.6	-9.8
158	$N \times \hat{\delta}$	1	1	0.0	1.0	-4.9	0.7	-0.4	-5.6
	$M3 \times \hat{\delta}$	4	1	1.0	0.8	-6.6	1.2	0.6	0.3
	$N \times \hat{D}_i$	3	1	0.0	0.6	-2.9	0.5	-0.3	-3.5

	$M3 \times \hat{D}_i$	4	1	0.0	0.8	-5.4	1.2	-0.6	-5.7
159	$N \times \hat{\delta}$	3	1	1.4	-1.0	-7.6	-0.3	0.7	6.7
	$M3 \times \hat{\delta}$	4	1	1.4	-1.5	-11.6	-0.5	1.2	10.2
	$N \times \hat{D}_i$	6	1	0.0	-2.8	-10.1	-0.5	1.6	-5.3
	$M3 \times \hat{D}_i$	4	1	0.0	-2.7	-12.0	-0.5	1.9	-6.3
160	$N \times \hat{\delta}$	2	1	3.1	0.2	-1.9	1.4	1.9	3.1
	$M3 \times \hat{\delta}$	1	1	3.1	-0.5	-2.7	1.5	1.8	3.9
	$N \times \hat{D}_i$	1	1	0.0	-3.7	-2.7	1.5	-3.0	-4.5
	$M3 \times \hat{D}_i$	4	1	0.0	-3.2	-3.0	1.5	-2.7	-4.5
161	$N \times \hat{\delta}$	6	1	0.5	1.8	-21.7	1.2	0.7	2.5
	$M3 \times \hat{\delta}$	1	1	0.5	1.7	-24.4	1.3	0.8	2.8
	$N \times \hat{D}_i$	3	1	0.0	0.8	-16.3	0.8	0.1	-6.2
	$M3 \times \hat{D}_i$	1	1	0.0	1.4	-24.4	1.3	0.2	-9.4
162	$N \times \hat{\delta}$	3	1	1.4	-1.0	-6.6	0.5	0.0	5.9
	$M3 \times \hat{\delta}$	4	1	1.4	-1.6	-10.3	0.7	-0.1	9.2
	$N \times \hat{D}_i$	6	1	0.0	-2.8	-8.8	0.7	-1.0	-4.5
	$M3 \times \hat{D}_i$	4	1	0.0	-2.7	-10.7	0.7	-1.1	-5.5
163	$N \times \hat{\delta}$	3	1	0.0	-3.9	8.8	-0.9	0.5	4.5
	$M3 \times \hat{\delta}$	1	1	0.0	-6.0	13.5	-1.4	0.7	6.9
	$N \times \hat{D}_i$	1	1	0.2	-6.0	13.4	-1.4	0.5	4.5

	$M3 \times \hat{D}_i$	1	1	1.1	-6.0	12.7	-1.4	-0.7	-7.1
164	$N \times \hat{\delta}$	1	1	0.0	5.5	7.8	1.0	-0.5	3.1
	$M3 \times \hat{\delta}$	4	1	0.0	5.1	9.2	0.2	-0.1	3.9
	$N \times \hat{D}_i$	3	1	0.0	3.6	5.2	0.6	-0.3	2.1
	$M3 \times \hat{D}_i$	4	1	1.1	5.1	8.4	0.2	0.1	-5.5
165	$N \times \hat{\delta}$	2	1	3.1	0.9	-1.3	-2.1	-2.8	2.3
	$M3 \times \hat{\delta}$	1	1	3.1	-1.0	-2.0	-2.4	-2.9	3.0
	$N \times \hat{D}_i$	1	1	0.0	-3.4	-2.0	-2.4	4.5	-3.3
	$M3 \times \hat{D}_i$	4	1	0.0	-2.0	-2.3	-2.3	4.2	-3.3
166	$N \times \hat{\delta}$	3	1	0.0	0.0	-7.7	-0.2	0.1	-4.8
	$M3 \times \hat{\delta}$	1	1	1.1	-0.1	-12.6	-0.3	-0.2	5.7
	$N \times \hat{D}_i$	2	1	0.0	-0.8	-9.1	-0.0	0.0	-5.8
	$M3 \times \hat{D}_i$	1	1	0.0	-0.1	-11.7	-0.3	0.1	-7.2
167	$N \times \hat{\delta}$	1	1	0.5	7.6	-12.9	-3.7	-1.9	2.2
	$M3 \times \hat{\delta}$	1	1	0.5	7.6	-12.9	-3.7	-1.9	2.2
	$N \times \hat{D}_i$	3	1	0.0	5.1	-8.3	-2.5	-0.0	-2.7
	$M3 \times \hat{D}_i$	4	1	0.0	7.3	-13.1	-3.0	-0.0	-4.4
168	$N \times \hat{\delta}$	1	1	0.0	1.2	-8.3	0.3	-0.1	-6.3
	$M3 \times \hat{\delta}$	4	1	1.1	0.7	-10.6	0.7	0.4	3.9
	$N \times \hat{D}_i$	2	1	0.0	0.5	-9.5	0.7	-0.4	-6.6

	$M3 \times \hat{D}_i$	4	1	0.0	0.7	-9.8	0.7	-0.3	-7.0
169	$N \times \hat{\delta}$	3	1	1.4	-5.3	-3.7	-1.3	-0.1	3.0
	$M3 \times \hat{\delta}$	4	1	1.4	-7.5	-6.0	-2.3	-0.2	4.9
	$N \times \hat{D}_i$	4	1	0.0	-8.5	-6.4	-2.3	3.0	-3.8
	$M3 \times \hat{D}_i$	4	1	0.0	-8.5	-6.4	-2.3	3.0	-3.8
170	$N \times \hat{\delta}$	2	1	3.1	-0.1	-1.2	3.7	5.5	2.2
	$M3 \times \hat{\delta}$	1	1	3.1	-2.0	-1.9	4.2	5.8	2.9
	$N \times \hat{D}_i$	1	1	0.0	-4.5	-1.9	4.2	-7.2	-3.1
	$M3 \times \hat{D}_i$	4	1	0.0	-3.1	-2.2	4.1	-6.7	-3.1
171	$N \times \hat{\delta}$	1	1	0.5	7.6	-11. 2	-2.4	-0.7	1.9
	$M3 \times \hat{\delta}$	1	1	0.5	7.6	-11. 2	-2.4	-0.7	1.9
	$N \times \hat{D}_i$	3	1	0.0	5.1	-7.1	-1.6	0.3	-2.4
	$M3 \times \hat{D}_i$	4	1	0.0	7.1	-11. 1	-2.7	0.4	-3.8
172	$N \times \hat{\delta}$	3	1	1.4	-5.0	-2.7	-1.0	-0.4	2.2
	$M3 \times \hat{\delta}$	4	1	1.4	-7.2	-4.7	-1.1	-0.5	3.9
	$N \times \hat{D}_i$	4	1	0.0	-8.1	-5.1	-1.1	1.1	-2.9
	$M3 \times \hat{D}_i$	4	1	0.0	-8.1	-5.1	-1.1	1.1	-2.9
173	$N \times \hat{\delta}$	1	1	0.0	40.9	77.7	5.7	-4.8	232. 7
	$M3 \times \hat{\delta}$	1	1	0.0	40.9	77.7	5.7	-4.8	232. 7
	$N \times \hat{D}_i$	2	1	0.2	20.8	63.5	4.2	-0.7	180. 5

	$M3 \times \hat{D}_i$	3	1	1.4	28.3	49.3	3.9	2.1	83.2
174	$N \times \hat{\delta}$	3	1	0.1	-12.5	45.3	-3.4	3.8	136.5
	$M3 \times \hat{\delta}$	4	1	0.0	-34.2	70.6	-5.5	7.8	216.2
	$N \times \hat{D}_i$	2	1	0.0	-34.9	63.9	-5.2	7.5	195.2
	$M3 \times \hat{D}_i$	3	1	1.4	-12.5	43.3	-3.4	-0.6	80.4
175	$N \times \hat{\delta}$	4	1	3.1	5.6	-6.0	1.5	3.7	9.7
	$M3 \times \hat{\delta}$	1	1	3.1	5.5	-6.6	1.6	4.0	10.2
	$N \times \hat{D}_i$	3	1	0.0	1.8	-4.4	1.1	-0.7	-6.9
	$M3 \times \hat{D}_i$	1	1	0.0	2.9	-6.6	1.6	-0.9	-10.3
176	$N \times \hat{\delta}$	4	1	1.4	3.3	-13.3	6.0	3.7	7.3
	$M3 \times \hat{\delta}$	4	1	1.4	3.3	-13.3	6.0	3.7	7.3
	$N \times \hat{D}_i$	3	1	0.0	1.2	-8.8	4.1	-3.6	-7.5
	$M3 \times \hat{D}_i$	4	1	0.0	2.3	-13.7	6.0	-4.8	-11.6
177	$N \times \hat{\delta}$	6	1	0.5	4.2	-13.8	9.2	10.5	6.3
	$M3 \times \hat{\delta}$	1	1	0.5	4.0	-15.1	10.2	10.9	6.9
	$N \times \hat{D}_i$	3	1	0.0	2.5	-10.1	6.8	3.9	-0.3
	$M3 \times \hat{D}_i$	1	1	0.0	3.8	-15.1	10.2	5.8	-0.7
178	$N \times \hat{\delta}$	5	1	1.4	0.0	0.0	0.0	0.0	-0.0
	$M3 \times \hat{\delta}$	2	1	1.4	-0.0	-0.0	0.0	0.0	0.0
	$N \times \hat{D}_i$	6	1	0.0	-0.8	0.0	0.0	0.0	0.0

	$M3 \times \hat{D}_i$	2	1	0.0	-0.8	-0.4	0.0	0.0	-0.3
179	$N \times \hat{\delta}$	3	1	3.1	-0.4	0.0	-0.0	-0.0	0.0
	$M3 \times \hat{\delta}$	1	1	0.0	-2.5	0.0	-0.0	0.0	0.0
	$N \times \hat{D}_i$	2	1	0.0	-2.5	-1.3	-0.0	0.0	-2.8
	$M3 \times \hat{D}_i$	2	1	0.0	-2.5	-1.3	-0.0	0.0	-2.8
180	$N \times \hat{\delta}$	3	1	0.5	-1.3	-0.0	0.0	0.0	0.0
	$M3 \times \hat{\delta}$	6	1	0.5	-2.5	-0.0	0.0	0.0	0.0
	$N \times \hat{D}_i$	4	1	0.0	-2.8	-1.3	0.0	0.0	-3.1
	$M3 \times \hat{D}_i$	2	1	0.0	-2.8	-1.4	0.0	0.0	-3.5
181	$N \times \hat{\delta}$	3	1	0.0	-0.0	3.5	-0.0	0.0	5.4
	$M3 \times \hat{\delta}$	6	1	0.0	-0.0	4.9	-0.0	0.0	7.9
	$N \times \hat{D}_i$	2	1	0.3	-0.0	4.7	1.4	-2.1	6.4
	$M3 \times \hat{D}_i$	2	1	1.8	-0.0	3.9	1.4	-0.0	-0.1
182	$N \times \hat{\delta}$	1	1	0.0	4.0	2.5	-3.8	3.2	-2.2
	$M3 \times \hat{\delta}$	3	1	0.0	2.7	2.7	-2.6	2.2	-1.4
	$N \times \hat{D}_i$	3	1	0.0	2.7	2.7	-2.6	2.2	-1.4
	$M3 \times \hat{D}_i$	1	1	0.0	4.0	2.5	-3.8	3.2	-2.2
183	$N \times \hat{\delta}$	2	1	0.4	-2.3	7.4	0.6	2.0	-7.0
	$M3 \times \hat{\delta}$	3	1	0.0	-2.5	6.1	0.8	0.9	-3.6
	$N \times \hat{D}_i$	1	1	0.2	-3.7	7.1	1.2	1.4	-7.8

	$M3 \times \hat{D}_i$	4	1	2.1	-2.6	4.7	0.8	3.5	-19.1
184	$N \times \hat{\delta}$	1	1	0.0	-0.0	0.0	-0.0	0.0	0.0
	$M3 \times \hat{\delta}$	2	1	1.9	-0.0	-1.1	-0.0	-0.0	1.0
	$N \times \hat{D}_i$	2	1	0.0	-0.0	0.0	-0.0	0.0	0.0
	$M3 \times \hat{D}_i$	6	1	0.0	-0.0	0.0	0.0	0.0	0.0
185	$N \times \hat{\delta}$	1	1	0.3	0.1	0.3	-0.1	0.1	0.3
	$M3 \times \hat{\delta}$	1	1	0.0	0.1	0.4	-0.1	0.1	0.4
	$N \times \hat{D}_i$	2	1	0.5	0.0	0.3	-0.0	0.0	0.2
	$M3 \times \hat{D}_i$	1	1	1.9	0.1	0.1	-0.1	-0.0	-0.1
186	$N \times \hat{\delta}$	2	1	0.6	0.0	0.3	-0.0	0.0	0.2
	$M3 \times \hat{\delta}$	1	1	0.0	-0.0	0.4	-0.0	0.0	0.5
	$N \times \hat{D}_i$	1	1	0.2	-0.0	0.4	-0.0	0.0	0.4
	$M3 \times \hat{D}_i$	1	1	1.9	-0.0	0.2	-0.0	0.0	-0.1
187	$N \times \hat{\delta}$	3	1	0.2	-0.2	2.7	2.0	-3.2	1.6
	$M3 \times \hat{\delta}$	4	1	0.0	-0.4	3.8	3.1	-5.4	2.8
	$N \times \hat{D}_i$	4	1	0.0	-0.4	3.8	3.1	-5.4	2.8
	$M3 \times \hat{D}_i$	4	1	1.9	-0.4	2.7	3.1	0.6	-3.4
188	$N \times \hat{\delta}$	1	1	0.0	3.7	-4.8	3.6	2.3	-2.0
	$M3 \times \hat{\delta}$	3	1	0.0	2.6	-3.9	2.5	1.6	-1.4
	$N \times \hat{D}_i$	3	1	0.0	2.6	-3.9	2.5	1.6	-1.4

	$M3 \times \hat{D}_i$	1	1	0.0	3.7	-4.8	3.6	2.3	-2.0
189	$N \times \hat{\delta}$	1	1	0.0	32.7	0.2	0.6	-1.0	0.5
	$M3 \times \hat{\delta}$	1	1	3.1	32.7	-1.5	0.6	0.9	2.5
	$N \times \hat{D}_i$	3	1	0.0	21.9	0.5	0.4	-0.7	0.5
	$M3 \times \hat{D}_i$	3	1	0.8	21.9	0.0	0.4	-0.4	0.3
190	$N \times \hat{\delta}$	1	1	0.3	52.6	0.4	-0.3	0.5	0.8
	$M3 \times \hat{\delta}$	1	1	3.2	52.6	-1.3	-0.3	-0.5	2.1
	$N \times \hat{D}_i$	3	1	0.0	35.7	0.7	-0.2	0.3	0.8
	$M3 \times \hat{D}_i$	3	1	1.3	35.7	-0.1	-0.2	0.1	0.4
191	$N \times \hat{\delta}$	2	1	0.0	-0.2	-0.2	-0.2	-0.0	-0.0
	$M3 \times \hat{\delta}$	3	1	0.0	-0.2	-0.2	-0.2	-0.0	-0.0
	$N \times \hat{D}_i$	1	1	0.0	-0.3	-0.3	-0.2	-0.0	-0.0
	$M3 \times \hat{D}_i$	1	1	0.0	-0.3	-0.3	-0.2	-0.0	-0.0
192	$N \times \hat{\delta}$	3	1	0.0	$-\frac{62}{5}$	0.7	0.2	-0.1	0.8
	$M3 \times \hat{\delta}$	1	1	3.2	$-\frac{92}{8}$	-1.3	0.3	0.9	2.2
	$N \times \hat{D}_i$	1	1	0.0	$-\frac{92}{8}$	0.5	0.3	-0.2	0.9
	$M3 \times \hat{D}_i$	3	1	1.1	$-\frac{62}{5}$	0.1	0.2	0.1	0.4
193	$N \times \hat{\delta}$	2	1	0.0	-0.0	-1.3	0.1	0.2	0.0
	$M3 \times \hat{\delta}$	3	1	0.0	-0.1	-2.8	-0.1	0.2	0.0
	$N \times \hat{D}_i$	1	1	0.0	-0.1	-0.8	-0.1	0.3	0.0

	$M3 \times \hat{D}_i$	1	1	0.0	-0.1	-0.8	-0.1	0.3	0.0
194	$N \times \hat{\delta}$	3	1	0.0	-0.3	-0.5	0.3	0.0	-0.0
	$M3 \times \hat{\delta}$	3	1	0.0	-0.3	-0.5	0.3	0.0	-0.0
	$N \times \hat{D}_i$	1	1	0.0	-0.5	-0.8	0.5	0.0	-0.0
	$M3 \times \hat{D}_i$	4	1	0.0	-0.4	-1.0	0.4	-0.0	-0.0
195	$N \times \hat{\delta}$	5	1	0.0	-0.0	0.1	-0.0	0.0	0.0
	$M3 \times \hat{\delta}$	4	1	0.0	-0.1	0.2	0.0	-0.0	0.0
	$N \times \hat{D}_i$	2	1	0.0	-0.1	0.1	0.0	-0.0	0.0
	$M3 \times \hat{D}_i$	1	1	1.2	-0.0	-0.0	-0.0	-0.0	-0.1
196	$N \times \hat{\delta}$	2	1	0.4	0.0	4.6	1.4	-1.9	5.8
	$M3 \times \hat{\delta}$	2	1	0.0	0.0	4.9	1.4	-2.5	8.0
	$N \times \hat{D}_i$	1	1	0.0	-0.0	4.9	0.0	-0.0	7.9
	$M3 \times \hat{D}_i$	6	1	1.8	0.0	3.9	0.0	0.0	0.0
197	$N \times \hat{\delta}$	3	1	0.0	-0.3	0.4	-0.1	0.1	0.3
	$M3 \times \hat{\delta}$	4	1	0.0	-0.3	0.4	-0.2	0.1	0.4
	$N \times \hat{D}_i$	1	1	0.0	-0.4	0.4	-0.2	0.1	0.4
	$M3 \times \hat{D}_i$	1	1	1.9	-0.4	0.1	-0.2	-0.3	-0.1
198	$N \times \hat{\delta}$	1	1	0.0	-0.0	-0.0	-0.0	-0.0	-0.0
	$M3 \times \hat{\delta}$	2	1	1.9	-0.0	-1.1	0.0	0.0	1.0
	$N \times \hat{D}_i$	2	1	0.0	-0.0	-0.0	0.0	0.0	-0.0

	$M3 \times \hat{D}_i$	2	1	0.0	-0.0	-0.0	0.0	0.0	-0.0
199	$N \times \hat{\delta}$	1	1	0.6	9.2	4.0	3.5	6.4	0.7
	$M3 \times \hat{\delta}$	1	1	0.0	9.2	4.3	3.5	4.1	3.4
	$N \times \hat{D}_i$	3	1	0.0	6.4	3.3	2.4	2.9	2.5
	$M3 \times \hat{D}_i$	1	1	1.9	9.2	3.3	3.5	10.8	-3.9
200	$N \times \hat{\delta}$	1	1	0.0	0.0	0.4	-0.0	0.1	0.5
	$M3 \times \hat{\delta}$	4	1	0.0	-0.0	0.4	-0.1	0.1	0.5
	$N \times \hat{D}_i$	2	1	0.0	-0.0	0.4	-0.1	0.1	0.5
	$M3 \times \hat{D}_i$	1	1	1.9	0.0	0.2	-0.0	0.0	-0.1
201	$N \times \hat{\delta}$	1	1	0.0	46.8	-0.1	0.0	-0.0	-0.2
	$M3 \times \hat{\delta}$	4	1	1.9	46.8	-0.4	0.0	0.0	0.3
	$N \times \hat{D}_i$	3	1	0.8	31.1	-0.1	0.0	-0.0	-0.0
	$M3 \times \hat{D}_i$	1	1	0.0	46.8	-0.1	0.0	-0.0	-0.2
202	$N \times \hat{\delta}$	1	1	0.0	46.2	0.8	-0.3	0.2	0.6
	$M3 \times \hat{\delta}$	1	1	0.0	46.2	0.8	-0.3	0.2	0.6
	$N \times \hat{D}_i$	3	1	0.0	30.7	0.6	-0.2	0.2	0.4
	$M3 \times \hat{D}_i$	4	1	1.3	46.0	0.6	-0.4	-0.2	-0.4
203	$N \times \hat{\delta}$	3	1	1.3	-12. 8	-0.2	0.0	0.0	0.1
	$M3 \times \hat{\delta}$	1	1	1.9	-19. 1	-0.4	0.0	0.0	0.3
	$N \times \hat{D}_i$	1	1	0.3	-19. 1	-0.2	0.0	-0.0	-0.2

	$M3 \times \hat{D}_i$	1	1	0.0	-19.1	-0.2	0.0	-0.0	-0.2
204	$N \times \hat{\delta}$	3	1	0.1	-12.7	0.6	0.0	-0.0	0.3
	$M3 \times \hat{\delta}$	4	1	0.0	-18.3	0.9	-0.1	0.1	0.6
	$N \times \hat{D}_i$	1	1	0.0	-18.9	0.9	0.1	-0.1	0.6
	$M3 \times \hat{D}_i$	4	1	1.3	-18.3	0.7	-0.1	-0.1	-0.5
205	$N \times \hat{\delta}$	3	1	0.0	-14.0	-0.1	0.0	-0.0	-0.2
	$M3 \times \hat{\delta}$	1	1	1.8	-21.0	-0.5	0.0	0.0	0.4
	$N \times \hat{D}_i$	1	1	0.3	-21.0	-0.3	0.0	-0.0	-0.2
	$M3 \times \hat{D}_i$	1	1	0.0	-21.0	-0.2	0.0	-0.1	-0.3
206	$N \times \hat{\delta}$	3	1	0.0	-13.2	0.5	-0.4	0.3	0.4
	$M3 \times \hat{\delta}$	4	1	0.0	-18.8	0.8	-0.3	0.2	0.6
	$N \times \hat{D}_i$	1	1	0.2	-19.9	0.7	-0.7	0.4	0.4
	$M3 \times \hat{D}_i$	4	1	1.3	-18.8	0.6	-0.3	-0.2	-0.4
207	$N \times \hat{\delta}$	4	1	0.0	50.1	-0.2	0.0	0.1	-0.2
	$M3 \times \hat{\delta}$	4	1	1.8	50.1	-0.5	0.0	0.1	0.4
	$N \times \hat{D}_i$	3	1	0.0	33.3	-0.1	-0.0	0.1	-0.1
	$M3 \times \hat{D}_i$	1	1	0.0	49.9	-0.2	-0.0	0.1	-0.2
208	$N \times \hat{\delta}$	1	1	0.1	47.9	0.8	1.1	-0.7	0.5
	$M3 \times \hat{\delta}$	1	1	0.0	47.9	0.8	1.1	-0.8	0.6
	$N \times \hat{D}_i$	3	1	0.0	32.0	0.6	0.7	-0.6	0.4

	$M3 \times \hat{D}_i$	1	1	1.3	47.9	0.6	1.1	0.6	-0.4
209	$N \times \hat{\delta}$	5	1	0.0	0.0	0.0	0.0	-0.0	0.0
	$M3 \times \hat{\delta}$	5	1	0.0	0.0	0.0	0.0	-0.0	0.0
	$N \times \hat{D}_i$	2	1	0.0	0.0	0.0	0.0	-0.0	0.0
	$M3 \times \hat{D}_i$	1	1	0.1	0.0	0.0	0.0	0.0	-0.0
210	$N \times \hat{\delta}$	3	1	0.0	-47. 7	0.5	-0.6	0.9	0.6
	$M3 \times \hat{\delta}$	1	1	3.1	-71. 2	-1.4	-0.9	-1.4	2.4
	$N \times \hat{D}_i$	1	1	0.3	-71. 2	0.2	-0.9	1.1	0.6
	$M3 \times \hat{D}_i$	3	1	1.0	-47. 7	-0.1	-0.6	0.3	0.4
211	$N \times \hat{\delta}$	1	1	0.0	0.0	0.0	-0.0	0.0	0.0
	$M3 \times \hat{\delta}$	2	1	0.0	0.0	0.1	-0.0	0.0	0.0
	$N \times \hat{D}_i$	2	1	0.0	0.0	0.1	-0.0	0.0	0.0
	$M3 \times \hat{D}_i$	4	1	0.1	0.0	0.0	-0.0	-0.0	-0.0
212	$N \times \hat{\delta}$	3	1	0.2	-21. 4	-3.1	1.5	-3.3	-2.8
	$M3 \times \hat{\delta}$	1	1	1.9	-31. 4	-5.6	2.3	-0.9	4.8
	$N \times \hat{D}_i$	1	1	0.3	-31. 4	-4.6	2.3	-4.6	-3.3
	$M3 \times \hat{D}_i$	4	1	0.0	-27. 4	-4.4	2.0	-4.8	-4.8
213	$N \times \hat{\delta}$	3	1	0.0	-8.4	-3.1	-1.5	0.9	-3.5
	$M3 \times \hat{\delta}$	1	1	1.9	-12. 1	-5.7	-2.2	-3.1	4.8
	$N \times \hat{D}_i$	1	1	0.0	-12. 1	-4.5	-2.2	1.3	-5.1

	$M3 \times \hat{D}_i$	1	1	0.0	-12.1	-4.5	-2.2	1.3	-5.1
214	$N \times \hat{\delta}$	3	1	0.0	-2.0	1.7	-0.2	0.4	0.8
	$M3 \times \hat{\delta}$	4	1	0.0	-3.1	2.7	-0.4	0.6	1.5
	$N \times \hat{D}_i$	4	1	0.0	-3.1	2.7	-0.4	0.6	1.5
	$M3 \times \hat{D}_i$	4	1	1.8	-3.1	1.7	-0.4	0.0	-2.4
215	$N \times \hat{\delta}$	4	1	0.0	5.7	13.5	5.5	1.0	-2.7
	$M3 \times \hat{\delta}$	3	1	0.0	3.8	9.3	3.7	0.7	-1.7
	$N \times \hat{D}_i$	3	1	0.0	3.8	9.3	3.7	0.7	-1.7
	$M3 \times \hat{D}_i$	4	1	0.0	5.7	13.5	5.5	1.1	-2.8
216	$N \times \hat{\delta}$	2	1	0.0	0.0	0.2	0.0	-0.0	0.0
	$M3 \times \hat{\delta}$	1	1	0.0	0.0	0.2	-0.0	0.0	0.0
	$N \times \hat{D}_i$	6	1	0.1	-0.0	0.1	-0.0	0.0	0.0
	$M3 \times \hat{D}_i$	1	1	1.2	0.0	-0.0	-0.0	-0.0	-0.1
217	$N \times \hat{\delta}$	3	1	0.0	-0.4	-3.8	1.3	-0.0	-0.0
	$M3 \times \hat{\delta}$	6	1	0.0	-0.5	-8.7	1.5	-0.0	-0.0
	$N \times \hat{D}_i$	4	1	0.0	-0.7	-10.0	5.4	0.1	-0.0
	$M3 \times \hat{D}_i$	4	1	0.0	-0.7	-10.0	5.4	0.1	-0.0
218	$N \times \hat{\delta}$	3	1	0.0	-0.4	0.5	-0.4	-0.0	-0.0
	$M3 \times \hat{\delta}$	3	1	0.0	-0.4	0.5	-0.4	-0.0	-0.0
	$N \times \hat{D}_i$	4	1	0.0	-0.6	0.8	-0.6	-0.0	-0.0

	$M3 \times \hat{D}_i$	1	1	0.0	-0.6	0.8	-0.5	-0.0	-0.0
219	$N \times \hat{\delta}$	1	1	0.0	0.1	0.1	0.1	-0.0	-0.0
	$M3 \times \hat{\delta}$	3	1	1.8	0.1	-0.2	0.0	0.0	0.1
	$N \times \hat{D}_i$	2	1	0.4	0.0	0.0	0.0	-0.0	-0.0
	$M3 \times \hat{D}_i$	1	1	0.7	0.1	0.0	0.1	0.0	-0.0
220	$N \times \hat{\delta}$	1	1	0.0	0.8	-11.9	-2.2	0.1	0.0
	$M3 \times \hat{\delta}$	4	1	0.0	0.2	-11.9	-1.5	0.1	0.0
	$N \times \hat{D}_i$	2	1	0.0	0.1	-9.7	-1.3	0.1	0.0
	$M3 \times \hat{D}_i$	3	1	0.0	0.5	-2.9	-1.8	0.0	-0.0
221	$N \times \hat{\delta}$	1	1	0.0	0.8	-0.1	0.8	0.0	-0.0
	$M3 \times \hat{\delta}$	3	1	0.0	0.6	-0.1	0.6	0.0	-0.0
	$N \times \hat{D}_i$	2	1	0.0	0.3	0.0	0.3	-0.0	-0.0
	$M3 \times \hat{D}_i$	1	1	0.0	0.8	-0.1	0.8	0.0	-0.0
222	$N \times \hat{\delta}$	3	1	0.0	-5.6	6.2	0.7	-2.0	-6.1
	$M3 \times \hat{\delta}$	3	1	0.0	-5.6	6.2	0.7	-2.0	-6.1
	$N \times \hat{D}_i$	4	1	0.2	-11.6	7.5	1.1	-3.1	-11.4
	$M3 \times \hat{D}_i$	1	1	2.1	-7.9	4.3	1.1	-0.6	-23.1
223	$N \times \hat{\delta}$	3	1	0.0	-4.1	1.4	1.4	0.5	-15.6
	$M3 \times \hat{\delta}$	3	1	0.0	-4.1	1.4	1.4	0.5	-15.6
	$N \times \hat{D}_i$	4	1	0.0	-6.3	6.6	3.8	0.8	-22.7

	$M3 \times \hat{D}_i$	1	1	0.0	-5.9	6.8	2.1	0.6	-22.9
224	$N \times \hat{\delta}$	4	1	2.7	16.1	1.6	3.2	2.5	-3.6
	$M3 \times \hat{\delta}$	4	1	0.0	15.6	3.5	2.7	-5.3	3.2
	$N \times \hat{D}_i$	3	1	0.2	10.7	2.2	2.0	-3.2	1.6
	$M3 \times \hat{D}_i$	4	1	2.7	16.1	1.6	3.2	2.5	-3.6
225	$N \times \hat{\delta}$	4	1	0.0	5.8	10.2	5.5	-1.5	-3.4
	$M3 \times \hat{\delta}$	3	1	0.0	3.9	7.5	3.5	-1.1	-2.2
	$N \times \hat{D}_i$	3	1	0.0	3.9	7.5	3.5	-1.0	-2.2
	$M3 \times \hat{D}_i$	4	1	0.0	5.8	10.2	5.5	-1.4	-3.5
226	$N \times \hat{\delta}$	2	1	2.7	3.0	-0.7	0.3	0.1	0.2
	$M3 \times \hat{\delta}$	1	1	0.0	0.3	1.1	-0.0	0.0	0.7
	$N \times \hat{D}_i$	6	1	0.4	0.3	0.7	-0.0	0.0	0.3
	$M3 \times \hat{D}_i$	1	1	1.5	0.3	0.0	-0.0	-0.0	-0.2
227	$N \times \hat{\delta}$	3	1	0.0	-0.4	-3.3	-1.2	0.0	-0.0
	$M3 \times \hat{\delta}$	1	1	0.0	-0.6	-9.5	-1.5	0.0	0.0
	$N \times \hat{D}_i$	4	1	0.0	-0.6	-9.2	-4.0	-0.0	0.0
	$M3 \times \hat{D}_i$	1	1	0.0	-0.6	-9.5	-1.5	0.0	-0.0
228	$N \times \hat{\delta}$	1	1	0.0	11.8	5.5	-3.7	8.8	-13.0
	$M3 \times \hat{\delta}$	3	1	0.0	8.1	4.5	-2.5	5.9	-8.0
	$N \times \hat{D}_i$	2	1	0.0	4.2	5.0	-3.1	6.2	-11.2

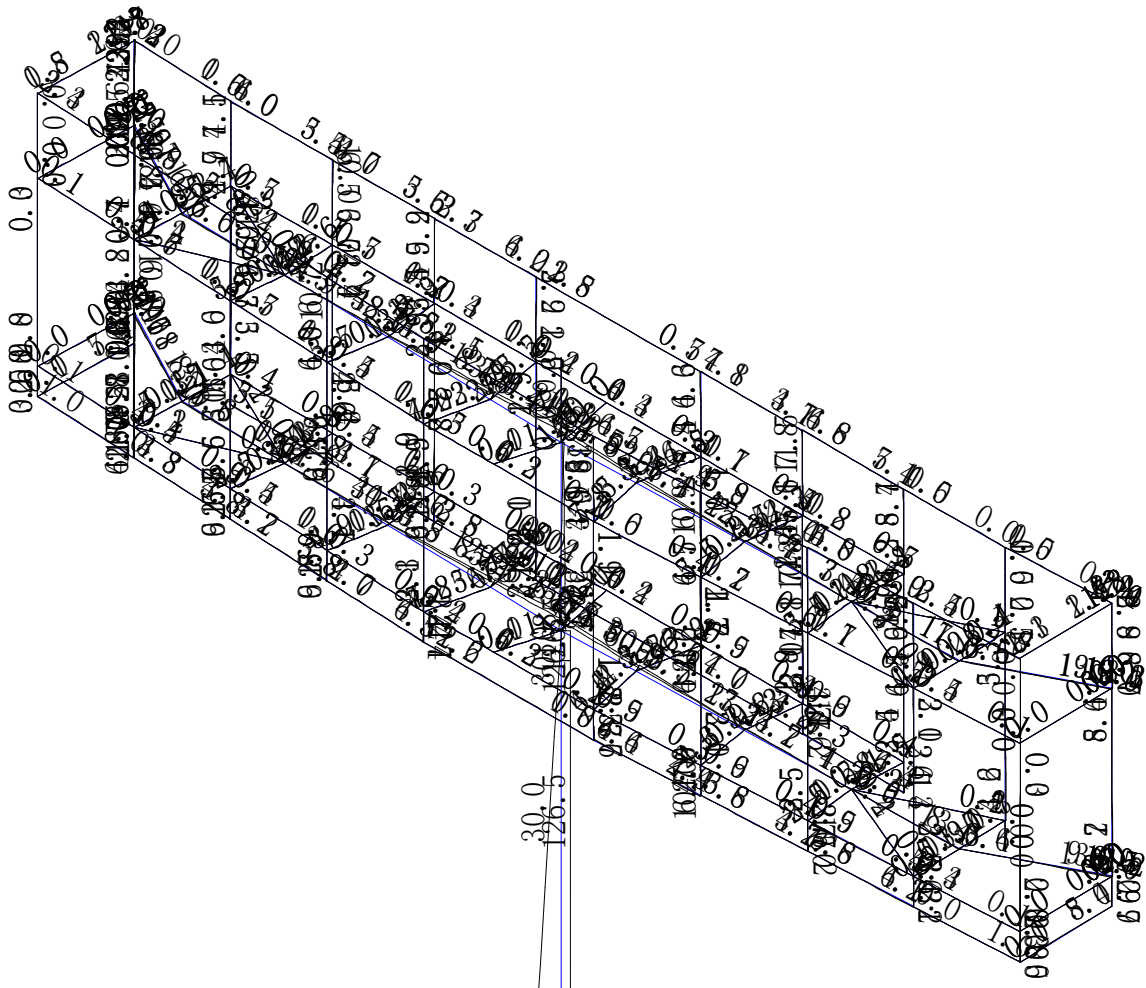
	$M3 \times \hat{i} \hat{D}_i$	1	1	2.1	11.8	1.9	-3.7	0.9	-20.8
229	$N \times \hat{i}' \hat{o}$	1	1	0.0	9.0	10.0	-5.0	-0.9	-20.6
	$M3 \times \hat{i}' \hat{o}$	3	1	0.0	6.0	1.6	-3.5	-0.6	-14.0
	$N \times \hat{i} \hat{D}_i$	2	1	0.0	2.8	8.1	-3.6	0.3	-18.2
	$M3 \times \hat{i} \hat{D}_i$	1	1	0.0	9.0	10.0	-5.0	-0.9	-20.7
230	$N \times \hat{i}' \hat{o}$	1	1	0.0	-0.3	0.9	-0.0	0.1	0.5
	$M3 \times \hat{i}' \hat{o}$	1	1	0.0	-0.3	0.9	-0.0	0.1	0.5
	$N \times \hat{i} \hat{D}_i$	2	1	0.0	-1.2	0.7	-0.3	0.2	0.4
	$M3 \times \hat{i} \hat{D}_i$	1	1	1.5	-0.3	-0.0	-0.0	0.0	-0.1
231	$N \times \hat{i}' \hat{o}$	1	1	0.0	0.8	-11.2	2.1	-0.0	-0.0
	$M3 \times \hat{i}' \hat{o}$	4	1	0.0	0.4	-11.1	1.4	-0.0	0.0
	$N \times \hat{i} \hat{D}_i$	2	1	0.0	0.2	-9.1	1.2	-0.0	0.0
	$M3 \times \hat{i} \hat{D}_i$	1	1	0.0	0.8	-11.2	2.1	-0.0	-0.0
232	$N \times \hat{i}' \hat{o}$	1	1	0.0	0.8	0.1	-0.8	-0.0	-0.0
	$M3 \times \hat{i}' \hat{o}$	3	1	0.0	0.6	0.1	-0.5	-0.0	-0.0
	$N \times \hat{i} \hat{D}_i$	2	1	0.0	0.3	-0.0	-0.3	0.0	-0.0
	$M3 \times \hat{i} \hat{D}_i$	1	1	0.0	0.8	0.1	-0.8	-0.0	-0.0
233	$N \times \hat{i}' \hat{o}$	2	1	0.0	0.5	1.1	-0.0	0.0	1.0
	$M3 \times \hat{i}' \hat{o}$	1	1	0.0	0.0	1.1	0.0	0.0	1.0
	$N \times \hat{i} \hat{D}_i$	2	1	1.9	-0.0	0.0	-0.0	-0.0	-0.0

	M3× îĐ _i	2	1	1.9	-0.0	0.0	-0.0	-0.0	-0.0
234	N×î 'ó	2	1	0.0	0.5	1.1	-0.0	0.0	1.0
	M3× î'ó	2	1	0.0	0.5	1.1	-0.0	0.0	1.0
	N× îĐ _i	1	1	0.0	0.0	1.1	-0.0	0.0	1.0
	M3× îĐ _i	2	1	1.9	0.0	0.0	-0.0	-0.0	-0.0
235	N×î 'ó	2	1	1.9	0.0	-0.0	-0.0	-0.0	0.0
	M3× î'ó	2	1	0.0	-0.5	1.1	-0.0	0.0	1.0
	N× îĐ _i	2	1	0.0	-0.5	1.1	-0.0	0.0	1.0
	M3× îĐ _i	1	1	1.9	-0.0	-0.0	-0.0	-0.0	-0.0

, ÷Đ § Ó_i × e° ïïÄ × î' óÖ § × ù · ' Á_i Êe¼EÖμ (μÏÎ»£° kN_i çkN. m)

节点号	ìÖÖÊ	组合号	组合序号	Nx	Ny	Nz	Mx	My	Mz
1	Nx×î' ó	6	1	0.0	-0.0	347. 2	30.5	109. 0	-0.0
	Ny×î' ó	2	1	-56. 4	0.0	347. 2	30.5	-876 .1	7.3
	Nz×î' ó	1	1	0.0	-0.0	379. 2	33.5	126. 5	-0.0
	Mx×î' ó	1	1	0.0	-0.0	379. 2	33.5	126. 5	-0.0
	My×î' ó	1	1	0.0	-0.0	379. 2	33.5	126. 5	-0.0
	Mz×î' ó	2	1	-56. 4	0.0	347. 2	30.5	-876 .1	7.3
	° ïïÄ _i × î'ó	4	1	-50. 8	0.0	376. 0	33.2	-761 .9	6.6
	Nx×îĐ _i	2	1	-56. 4	0.0	347. 2	30.5	-876 .1	7.3
	Ny×îĐ _i	1	1	0.0	-0.0	379. 2	33.5	126. 5	-0.0

$N_z \times \hat{i}$	3	1	0.0	-0.0	288. 8	22.9	73.9	-0.0
$M_x \times \hat{i}$	3	1	0.0	-0.0	288. 8	22.9	73.9	-0.0
$M_y \times \hat{i}$	2	1	-56. 4	0.0	347. 2	30.5	-876 .1	7.3
$M_z \times \hat{i}$	1	1	0.0	-0.0	379. 2	33.5	126. 5	-0.0



876.1

126.5



Íä¼à M3 ° üÂÇÍ¼(μ¥Î»£° kN. m)

ÖäÁ! N × î´óμÄÇ° 10 , öμ¥Ôª μÄÄÜÁ! (μ¥Î»£° M, KN, KN. M)

序号	单元号	组合号	组合序	位置	轴力N	剪力Q2	剪力Q3	扭矩M	弯距M2	弯距M3
1	80	4	1	0.00 0	53.8	62.1	-3.6	-2.2	3.9	175.3
2	190	1	1	0.26 9	52.6	0.4	-0.3	-0.2	0.5	0.8
3	207	4	1	0.00 0	50.1	-0.2	0.0	0.0	0.1	-0.2
4	208	1	1	0.11 1	47.9	0.8	1.1	-0.0	-0.7	0.5
5	31	4	1	0.00 0	47.2	37.9	-0.2	-3.5	-2.1	95.5
6	150	1	1	0.00 0	47.1	-4.8	0.3	0.3	-0.2	-4.0
7	201	1	1	0.00 0	46.8	-0.1	0.0	0.0	-0.0	-0.2
8	202	1	1	0.00 0	46.2	0.8	-0.3	-0.0	0.2	0.6
9	23	4	1	0.00 0	45.2	6.2	-0.0	-0.7	-0.1	6.5
10	148	1	1	0.00 0	43.1	-45.4	0.3	2.3	-2.9	34.5

ÖäÁ! N × îÐ; μÄÇ° 10 , öμ¥Ôª μÄÄÜÁ! (μ¥Î»£° M, KN, KN. M)

序号	单元号	组合号	组合序	位置	轴力N	剪力Q2	剪力Q3	扭矩M	弯距M2	弯距M3
1	1	1	1	0.00 0	-379.2	0.0	-0.0	-0.0	33.5	126.5
2	3	1	1	0.00 0	-295.4	0.0	-0.0	-0.0	33.5	126.5
3	4	1	1	3.10 0	-154.2	-9.4	-7.3	1.6	-26.3	59.7
4	192	1	1	0.00 0	-92.8	0.5	0.3	0.1	-0.2	0.9
5	149	1	1	0.00 0	-80.1	-4.8	-0.0	0.3	-0.6	-4.0
6	27	1	1	0.00	-74.2	-5.1	-1.2	-0.6	1.6	-4.4

				0						
7	210	1	1	0.26 0	-71.2	0.2	-0.9	-0.1	1.1	0.6
8	146	1	1	0.00 0	-60.0	-4.5	1.5	0.4	-1.6	-3.8
9	98	1	1	0.00 0	-54.8	-4.8	0.4	0.2	-1.1	-4.7
10	48	1	1	0.16 1	-50.3	6.6	0.6	-0.3	-2.5	5.9

Íä¼à M3 × î´óμÄÇ° 10 , öμΥÔª μÄÄÚÁ! (μΥÎ»£° M, KN, KN. M)

序号	单元号	组合号	组合序	位置	轴力N	剪力Q2	剪力Q3	扭矩M	弯距M2	弯距M3
1	173	1	1	0.00 0	40.9	77.7	5.7	1.2	-4.8	232.7
2	174	4	1	0.00 0	-34.2	70.6	-5.5	2.7	7.8	216.2
3	81	1	1	0.00 0	-25.5	67.6	2.6	-3.7	-4.2	184.5
4	80	4	1	0.00 0	53.8	62.1	-3.6	-2.2	3.9	175.3
5	148	1	1	2.00 0	43.1	-49.5	0.3	2.3	-2.2	129.5
6	147	1	1	2.00 0	-19.4	-48.6	-1.2	2.9	0.1	127.0
7	1	1	1	0.00 0	-379.2	0.0	-0.0	-0.0	33.5	126.5
8	3	1	1	0.00 0	-295.4	0.0	-0.0	-0.0	33.5	126.5
9	34	1	1	0.00 0	-23.3	41.3	0.5	-4.0	-0.2	98.4
10	31	4	1	0.00 0	47.2	37.9	-0.2	-3.5	-2.1	95.5

Íä¼à M3 × îÐ; μÄÇ° 10 , öμΥÔª μÄÄÚÁ! (μΥÎ»£° M, KN, KN. M)

序号	单元号	组合号	组合序	位置	轴力N	剪力Q2	剪力Q3	扭矩M	弯距M2	弯距M3
1	1	2	1	0.00 0	-347.2	-56.4	0.0	7.3	30.5	-876.1
2	4	2	1	3.10	-138.4	23.9	-6.7	4.2	-24.0	-37.3

				0						
3	3	2	1	0.00 0	-263.4	-56.4	0.0	7.3	30.5	-30.0
4	125	4	1	0.00 0	-11.0	-11.6	0.5	4.5	3.1	-26.0
5	222	1	1	2.13 6	-7.9	4.3	1.1	-2.1	-0.6	-23.1
6	223	1	1	0.00 6	-5.9	6.8	2.1	-2.0	0.6	-22.9
7	118	4	1	0.00 0	5.0	-8.7	0.9	6.2	-6.9	-21.6
8	228	1	1	2.13 6	11.8	1.9	-3.7	2.4	0.9	-20.8
9	229	1	1	0.00 6	9.0	10.0	-5.0	2.4	-0.9	-20.7
10	135	4	1	0.00 0	-2.1	-6.8	0.5	-0.5	-3.5	-19.2

(二). 位移

1. 工况位移

2. 组合位移

° Xİöİ»òEi ±×î´óµÄÇ° 10 , ö¼ÚµäÎ»òE±í £ ¨ µ¶Î»£° mm£©

序号	节点号	组合号	组合序号	X向位移	Y向位移	Z向位移	位移平方和
1	56	2	1	54.3	-17.2	-41.7	70.6
2	54	2	1	43.7	-11.8	-41.7	61.6
3	105	2	1	35.2	-15.2	-7.1	38.9
4	133	2	1	33.7	1.3	-37.9	50.8
5	42	2	1	33.7	1.4	-28.7	44.3
6	58	2	1	31.8	1.0	-36.8	48.6
7	131	2	1	31.8	1.0	-36.7	48.6
8	130	2	1	31.8	1.0	-36.7	48.6
9	5	2	1	30.8	2.3	-0.4	30.9
10	111	2	1	30.7	1.0	-36.0	47.3

° Yİöİ»òEi ±×î´óµÄÇ° 10 , ö¼ÚµäÎ»òE±í £ ¨ µ¶Î»£° mm£©

序号	节点号	组合号	组合序号	X向位移	Y向位移	Z向位移	位移平方和
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1	56	2	1	54.3	-17.2	-41.7	70.6
2	105	6	1	-16.3	-16.3	-33.4	40.5
3	54	2	1	43.7	-11.8	-41.7	61.6
4	104	6	1	-12.8	-11.1	-33.4	37.4
5	70	4	1	25.4	2.9	-3.2	25.8
6	68	4	1	25.4	2.9	-5.9	26.2
7	102	4	1	18.1	2.9	-12.4	22.2
8	100	4	1	18.7	2.9	-8.0	20.6
9	79	4	1	25.2	2.8	-3.6	25.6
10	108	4	1	18.0	2.8	-8.0	19.9

10, 10, 10, 10, 10, 10, 10, 10, 10, 10

序号	节点号	组合号	组合序号	X向位移	Y向位移	Z向位移	位移平方和
1	56	2	1	54.3	-17.2	-41.7	70.6
2	54	2	1	43.7	-11.8	-41.7	61.6
3	53	2	1	22.3	0.0	-41.7	47.3
4	52	2	1	19.6	1.9	-41.7	46.2
5	133	2	1	33.7	1.3	-37.9	50.8
6	113	2	1	21.9	1.8	-37.1	43.1
7	47	2	1	19.2	1.9	-36.8	41.5
8	55	2	1	21.4	1.8	-36.8	42.6
9	57	2	1	28.1	1.1	-36.8	46.3
10	58	2	1	31.8	1.0	-36.8	48.6

10, 10, 10, 10, 10, 10, 10, 10, 10, 10

序号	节点号	组合号	组合序号	X向位移	Y向位移	Z向位移	位移平方和
1	56	2	1	54.3	-17.2	-41.7	70.6
2	54	2	1	43.7	-11.8	-41.7	61.6
3	133	2	1	33.7	1.3	-37.9	50.8
4	58	2	1	31.8	1.0	-36.8	48.6
5	131	2	1	31.8	1.0	-36.7	48.6
6	130	2	1	31.8	1.0	-36.7	48.6
7	111	2	1	30.7	1.0	-36.0	47.3
8	53	2	1	22.3	0.0	-41.7	47.3
9	57	2	1	28.1	1.1	-36.8	46.3
10	127	2	1	28.1	1.1	-36.7	46.3

五、设计验算结果

本工程有1种材料：Q235钢(A3钢)

设计验算结果表 (强度和整体稳定为(应力/设计强度))

单元号	强度	绕2轴整体稳定	绕3轴整体稳定	绕2轴抗剪应力比	绕3轴抗剪应力比	绕2轴长细比	绕3轴长细比	绕2轴W/1	绕3轴W/1	结果
1	0.27	0.27	0.27	0.00	0.00	35	35	1/459 43	0	满足
2	0.00	0.00	0.00	0.00	0.00	4	4	1/488	1/425 5	满足
3	0.11	0.11	0.11	0.00	0.00	1	1	0	0	满足
4	0.05	0.06	0.06	0.00	0.00	9	9	0	0	满足
5	0.18	0.18	0.19	0.08	0.00	37	10	0	0	满足
6	0.22	0.22	0.24	0.07	0.01	37	10	0	0	满足
7	0.17	0.17	0.18	0.05	0.01	35	10	0	0	满足
8	0.23	0.23	0.27	0.04	0.01	35	10	0	0	满足
9	0.22	0.22	0.25	0.04	0.01	33	9	0	0	满足
10	0.16	0.16	0.17	0.05	0.01	33	9	0	0	满足
11	0.13	0.13	0.14	0.02	0.01	31	9	0	0	满足
12	0.06	0.06	0.06	0.01	0.00	31	9	0	0	满足
13	0.19	0.19	0.19	0.01	0.00	38	116	0	0	满足
14	0.21	0.21	0.25	0.01	0.00	38	116	0	0	满足
15	0.2	0.32	0.29	0.03	0.01	12	53	0	0	满足

	9									
16	0.2 2	0.40	0.33	0.03	0.00	33	103	0	0	满足
17	0.2 0	0.43	0.38	0.03	0.00	33	103	0	0	满足
18	0.1 8	0.40	0.39	0.02	0.00	33	103	0	0	满足
19	0.0 3	0.04	0.04	0.00	0.00	31	95	0	0	满足
20	0.1 9	0.36	0.36	0.02	0.00	33	103	0	0	满足
21	0.1 7	0.32	0.27	0.02	0.00	33	103	0	0	满足
22	0.2 2	0.22	0.22	0.02	0.00	33	103	0	0	满足
23	0.2 2	0.31	0.25	0.03	0.00	12	53	0	0	满足
24	0.2 4	0.28	0.24	0.03	0.00	12	53	0	1/441 92	满足
25	0.2 8	0.30	0.28	0.03	0.00	12	53	0	1/226 56	满足
26	0.2 5	0.34	0.30	0.03	0.00	12	53	0	1/304 03	满足
27	0.2 5	0.40	0.36	0.03	0.00	12	53	0	1/371 48	满足
28	0.1 8	0.29	0.25	0.10	0.01	3	14	0	0	满足
29	0.1 0	0.10	0.10	0.01	0.00	19	86	0	0	满足
30	0.2 7	0.27	0.27	0.04	0.01	9	39	0	0	满足
31	0.2 4	0.24	0.24	0.00	0.00	11	11	1/432 1	0	满足
32	0.0 9	0.09	0.09	0.00	0.00	11	11	1/787 6	0	满足
33	0.0 4	0.05	0.05	0.00	0.00	11	11	0	0	满足
34	0.2 4	0.24	0.24	0.00	0.00	11	11	1/431 9	0	满足
35	0.0	0.09	0.09	0.00	0.00	11	11	1/794	0	满足

	9							5		
36	0.0 4	0.05	0.05	0.00	0.00	11	11	0	0	满足
37	0.1 7	0.51	0.42	0.14	0.00	3	14	0	0	满足
38	0.1 3	0.17	0.17	0.01	0.01	19	86	0	0	满足
39	0.4 4	0.44	0.44	0.06	0.00	9	39	0	0	满足
40	0.1 7	0.53	0.44	0.14	0.01	3	14	0	0	满足
41	0.1 6	0.20	0.20	0.01	0.01	19	86	0	0	满足
42	0.4 6	0.46	0.46	0.07	0.00	9	39	0	0	满足
43	0.1 5	0.19	0.19	0.01	0.00	19	86	0	0	满足
44	0.4 1	0.41	0.41	0.06	0.00	9	39	0	0	满足
45	0.2 0	0.20	0.21	0.08	0.01	37	10	0	0	满足
46	0.3 1	0.31	0.36	0.07	0.02	37	10	0	0	满足
47	0.0 9	0.11	0.12	0.01	0.01	19	86	0	0	满足
48	0.2 6	0.41	0.36	0.03	0.00	12	53	0	1/413 52	满足
49	0.2 4	0.24	0.24	0.02	0.00	33	103	0	0	满足
50	0.1 9	0.32	0.27	0.11	0.00	3	14	0	0	满足
51	0.2 2	0.35	0.29	0.04	0.00	12	53	0	0	满足
52	0.2 0	0.43	0.41	0.03	0.00	33	103	0	0	满足
53	0.3 0	0.30	0.30	0.04	0.00	9	39	0	0	满足
54	0.3 0	0.36	0.31	0.04	0.01	12	53	0	1/413 52	满足
55	0.3	0.34	0.33	0.04	0.00	12	53	0	0	满足

	3									
56	0.2 2	0.46	0.41	0.03	0.00	33	103	0	0	满足
57	0.1 8	0.32	0.28	0.02	0.00	33	103	0	0	满足
58	0.1 1	0.15	0.14	0.01	0.00	19	86	0	0	满足
59	0.3 7	0.37	0.42	0.05	0.03	35	10	0	0	满足
60	0.2 1	0.57	0.48	0.16	0.01	3	14	0	0	满足
61	0.1 9	0.19	0.21	0.05	0.01	35	10	0	0	满足
62	0.5 0	0.50	0.50	0.07	0.00	9	39	0	0	满足
63	0.0 8	0.11	0.12	0.01	0.00	38	116	0	0	满足
64	0.2 0	0.20	0.22	0.03	0.01	33	9	0	0	满足
65	0.4 1	0.41	0.49	0.02	0.03	33	9	0	0	满足
66	0.0 7	0.09	0.08	0.01	0.00	38	116	0	0	满足
67	0.1 3	0.18	0.16	0.01	0.00	19	86	0	0	满足
68	0.1 5	0.33	0.29	0.10	0.01	3	14	0	0	满足
69	0.3 7	0.37	0.37	0.05	0.00	9	39	0	0	满足
70	0.0 1	0.01	0.01	0.01	0.01	0	0	0	0	满足
71	0.1 5	0.15	0.15	0.07	0.01	0	0	0	0	满足
72	0.2 4	0.24	0.24	0.02	0.00	19	86	0	0	满足
73	0.0 8	0.08	0.08	0.03	0.00	31	9	0	0	满足
74	0.0 4	0.04	0.04	0.01	0.00	31	9	1/748 00	0	满足
75	0.0	0.09	0.09	0.00	0.00	9	39	0	0	满足

	9									
76	0.15	0.32	0.27	0.10	0.00	3	14	0	0	满足
77	0.00	0.00	0.00	0.00	0.00	3	14	1/311	1/383 48	满足
78	0.01	0.01	0.01	0.00	0.00	0	95	0	0	满足
79	0.01	0.01	0.01	0.04	0.01	0	95	0	0	满足
80	0.43	0.43	0.43	0.00	0.00	8	8	1/480 6	0	满足
81	0.44	0.45	0.45	0.00	0.00	8	8	1/477 8	0	满足
82	0.06	0.06	0.06	0.01	0.00	37	10	0	0	满足
83	0.15	0.15	0.15	0.01	0.01	39	11	0	0	满足
84	0.08	0.08	0.08	0.01	0.00	39	11	0	0	满足
85	0.04	0.04	0.04	0.01	0.00	37	10	0	0	满足
86	0.12	0.12	0.12	0.01	0.00	19	86	1/144	1/262	满足
87	0.15	0.15	0.15	0.01	0.00	3	14	1/144	1/266	满足
88	0.01	0.01	0.01	0.00	0.00	9	39	1/144	1/262	满足
89	0.39	0.44	0.41	0.03	0.01	19	86	0	0	满足
90	0.08	0.13	0.13	0.01	0.00	3	14	0	0	满足
91	0.18	0.46	0.39	0.05	0.01	9	39	0	0	满足
92	0.18	0.30	0.24	0.02	0.00	33	103	0	0	满足
93	0.22	0.45	0.41	0.03	0.00	33	103	0	0	满足
94	0.22	0.27	0.23	0.03	0.00	12	53	0	1/179 60	满足
95	0.2	0.32	0.28	0.03	0.00	12	53	0	1/473	满足

	3								76	
96	0.1 2	0.12	0.12	0.00	0.00	11	11	1/655 6	0	满足
97	0.1 2	0.12	0.12	0.00	0.00	11	11	1/637 0	0	满足
98	0.2 5	0.34	0.30	0.03	0.00	12	53	0	1/519 49	满足
99	0.2 5	0.29	0.25	0.03	0.00	12	53	0	1/476 11	满足
100	0.1 9	0.31	0.26	0.02	0.00	33	103	0	0	满足
101	0.2 4	0.48	0.43	0.03	0.00	33	103	0	0	满足
102	0.0 1	0.01	0.01	0.04	0.01	0	0	0	0	满足
103	0.0 3	0.04	0.04	0.00	0.00	0	0	0	0	满足
104	0.1 7	0.18	0.18	0.01	0.01	16	73	0	0	满足
105	0.0 3	0.04	0.04	0.00	0.00	12	12	0	0	满足
106	0.0 1	0.01	0.01	0.04	0.00	0	0	0	0	满足
107	0.0 9	0.09	0.09	0.02	0.01	0	49	0	0	满足
108	0.1 8	0.18	0.18	0.02	0.02	11	49	0	0	满足
109	0.1 3	0.18	0.20	0.01	0.00	38	116	0	0	满足
110	0.0 9	0.09	0.09	0.05	0.00	33	9	0	0	满足
111	0.0 7	0.07	0.07	0.03	0.00	33	9	0	0	满足
112	0.1 2	0.12	0.12	0.01	0.00	38	116	0	0	满足
113	0.0 8	0.08	0.08	0.02	0.00	31	9	0	0	满足
114	0.0 9	0.09	0.09	0.01	0.00	31	9	0	0	满足
115	0.2	0.24	0.24	0.02	0.00	19	86	0	0	满足

	4									
116	0.2 6	0.26	0.26	0.02	0.00	19	86	0	0	满足
117	0.0 1	0.01	0.01	0.02	0.01	0	0	0	0	满足
118	0.0 6	0.07	0.07	0.00	0.00	11	11	0	0	满足
119	0.1 6	0.33	0.30	0.02	0.00	33	103	0	0	满足
120	0.1 3	0.13	0.13	0.01	0.00	38	116	0	0	满足
121	0.0 7	0.07	0.07	0.02	0.00	31	9	0	0	满足
122	0.3 1	0.31	0.31	0.08	0.02	3	14	0	0	满足
123	0.1 3	0.13	0.14	0.03	0.01	33	9	0	0	满足
124	0.4 1	0.41	0.41	0.12	0.00	3	14	0	0	满足
125	0.0 6	0.07	0.07	0.00	0.00	11	11	0	0	满足
126	0.3 1	0.32	0.31	0.03	0.01	12	53	0	1/540 06	满足
127	0.2 4	0.43	0.37	0.03	0.00	33	103	0	0	满足
128	0.1 5	0.20	0.22	0.01	0.00	38	116	0	0	满足
129	0.2 9	0.50	0.44	0.06	0.00	9	39	0	0	满足
130	0.0 9	0.09	0.09	0.04	0.00	31	9	0	0	满足
131	0.1 5	0.15	0.16	0.04	0.00	33	9	0	0	满足
132	0.3 1	0.57	0.49	0.07	0.01	9	39	0	0	满足
133	0.2 3	0.24	0.23	0.02	0.00	19	86	0	0	满足
134	0.2 3	0.23	0.23	0.02	0.00	19	86	0	0	满足
135	0.0	0.05	0.05	0.00	0.00	0	0	0	0	满足

	5									
136	0.1 5	0.32	0.29	0.02	0.00	33	103	0	0	满足
137	0.2 3	0.23	0.23	0.06	0.01	3	14	0	0	满足
138	0.4 1	0.41	0.41	0.12	0.01	3	14	0	0	满足
139	0.2 1	0.40	0.34	0.03	0.00	33	103	0	0	满足
140	0.2 7	0.28	0.27	0.03	0.00	12	53	0	1/179 60	满足
141	0.2 1	0.36	0.31	0.04	0.00	9	39	0	0	满足
142	0.2 7	0.52	0.44	0.06	0.00	9	39	0	0	满足
143	0.1 9	0.40	0.40	0.02	0.00	33	103	0	0	满足
144	0.1 8	0.30	0.25	0.03	0.00	12	53	0	1/179 60	满足
145	0.2 3	0.23	0.23	0.02	0.00	33	103	0	0	满足
146	0.2 1	0.37	0.33	0.03	0.00	12	53	0	1/343 98	满足
147	0.3 0	0.31	0.31	0.00	0.00	11	11	1/324 2	0	满足
148	0.3 2	0.32	0.32	0.00	0.00	11	11	1/316 9	0	满足
149	0.2 4	0.39	0.36	0.03	0.00	12	53	0	1/639 81	满足
150	0.2 2	0.31	0.25	0.03	0.00	12	53	0	0	满足
151	0.2 3	0.23	0.23	0.02	0.00	33	103	0	0	满足
152	0.1 9	0.42	0.41	0.03	0.00	33	103	0	0	满足
153	0.0 9	0.09	0.09	0.04	0.00	35	10	0	0	满足
154	0.1 0	0.10	0.11	0.05	0.00	35	10	0	0	满足
155	0.2	0.22	0.22	0.02	0.00	19	86	0	0	满足

	2									
156	0.1 5	0.15	0.16	0.05	0.01	35	10	0	0	满足
157	0.4 2	0.42	0.42	0.13	0.00	3	14	0	0	满足
158	0.1 6	0.16	0.17	0.04	0.00	35	10	0	1/771 03	满足
159	0.2 8	0.52	0.44	0.06	0.00	9	39	0	0	满足
160	0.2 1	0.21	0.21	0.02	0.00	19	86	0	0	满足
161	0.4 0	0.40	0.40	0.13	0.00	3	14	0	0	满足
162	0.2 4	0.47	0.40	0.06	0.00	9	39	0	0	满足
163	0.2 1	0.21	0.23	0.09	0.01	37	10	0	0	满足
164	0.1 4	0.14	0.14	0.06	0.00	37	10	0	0	满足
165	0.1 6	0.17	0.18	0.01	0.01	19	86	0	0	满足
166	0.1 4	0.14	0.14	0.08	0.00	37	10	0	0	满足
167	0.2 0	0.20	0.20	0.07	0.01	3	14	0	0	满足
168	0.1 6	0.16	0.16	0.07	0.00	37	10	0	0	满足
169	0.1 8	0.27	0.23	0.03	0.01	9	39	0	0	满足
170	0.1 7	0.18	0.20	0.01	0.01	19	86	0	0	满足
171	0.1 7	0.17	0.17	0.06	0.01	3	14	0	0	满足
172	0.1 3	0.21	0.18	0.03	0.00	9	39	0	0	满足
173	0.5 6	0.56	0.56	0.00	0.00	8	8	1/338 2	0	满足
174	0.5 2	0.53	0.53	0.00	0.00	8	8	1/349 5	0	满足
175	0.4	0.53	0.47	0.04	0.00	19	86	0	0	满足

	6									
176	0.5 2	0.52	0.52	0.07	0.02	9	39	0	0	满足
177	0.1 6	0.37	0.35	0.08	0.03	3	14	1/835 1	0	满足
178	0.0 1	0.01	0.01	0.00	0.00	9	39	1/357	1/270	满足
179	0.1 2	0.12	0.12	0.01	0.00	19	86	1/357	1/270	满足
180	0.1 5	0.15	0.15	0.01	0.00	3	14	1/357	1/276	满足
181	0.1 3	0.41	0.35	0.03	0.00	11	49	0	0	满足
182	0.1 1	0.11	0.11	0.01	0.01	0	0	0	0	满足
183	0.0 5	0.05	0.05	0.00	0.00	12	12	0	0	满足
184	0.0 2	0.05	0.04	0.01	0.00	12	53	1/434	1/355 5	满足
185	0.0 6	0.14	0.12	0.01	0.00	33	102	0	0	满足
186	0.0 7	0.17	0.14	0.01	0.00	33	102	0	0	满足
187	0.1 7	0.17	0.17	0.02	0.01	12	53	0	0	满足
188	0.1 0	0.10	0.10	0.02	0.01	0	0	0	0	满足
189	0.0 7	0.09	0.12	0.01	0.00	91	86	0	1/179 60	满足
190	0.0 8	0.08	0.08	0.01	0.00	20	89	0	0	满足
191	0.0 1	0.01	0.01	0.00	0.00	0	0	0	0	满足
192	0.1 1	0.17	0.22	0.01	0.00	20	89	0	0	满足
193	0.0 2	0.02	0.02	0.05	0.00	0	95	0	0	满足
194	0.0 1	0.01	0.01	0.02	0.01	0	95	0	0	满足
195	0.0	0.02	0.02	0.00	0.00	31	95	1/171	0	满足

	2							51		
196	0.1 3	0.36	0.35	0.03	0.00	11	49	0	0	满足
197	0.0 7	0.16	0.14	0.01	0.00	33	102	0	0	满足
198	0.0 2	0.05	0.04	0.01	0.00	12	53	1/218	1/514 7	满足
199	0.2 3	0.23	0.41	0.02	0.01	48	53	0	1/203 08	满足
200	0.0 7	0.18	0.15	0.01	0.00	33	102	0	0	满足
201	0.1 9	0.19	0.19	0.01	0.00	33	172	0	0	满足
202	0.2 7	0.27	0.27	0.01	0.00	23	172	0	0	满足
203	0.1 2	0.19	0.36	0.01	0.00	33	172	0	0	满足
204	0.1 9	0.27	0.44	0.02	0.00	23	172	0	0	满足
205	0.1 5	0.21	0.38	0.01	0.00	31	166	0	0	满足
206	0.1 9	0.28	0.45	0.01	0.01	23	166	0	0	满足
207	0.2 2	0.22	0.22	0.01	0.00	31	166	0	0	满足
208	0.3 0	0.30	0.30	0.01	0.02	23	166	0	1/387 23	满足
209	0.0 0	0.00	0.00	0.00	0.00	2	6	1/570	1/124 36	满足
210	0.1 0	0.18	0.22	0.01	0.00	44	86	0	1/331 05	满足
211	0.0 0	0.00	0.00	0.00	0.00	44	3	1/503	1/331 05	满足
212	0.2 5	0.30	0.27	0.03	0.01	12	53	0	0	满足
213	0.2 4	0.27	0.24	0.03	0.01	12	53	0	0	满足
214	0.1 1	0.11	0.11	0.01	0.00	11	49	0	0	满足
215	0.1	0.13	0.13	0.07	0.01	0	49	0	0	满足

	3									
216	0.0 2	0.02	0.02	0.00	0.00	31	95	1/147 97	0	满足
217	0.0 2	0.02	0.02	0.18	0.07	0	95	0	0	满足
218	0.0 1	0.01	0.01	0.01	0.01	0	95	0	0	满足
219	0.0 2	0.03	0.03	0.00	0.00	31	95	1/174 90	0	满足
220	0.0 1	0.02	0.02	0.20	0.03	0	95	0	0	满足
221	0.0 1	0.01	0.01	0.00	0.01	0	95	0	0	满足
222	0.0 6	0.06	0.06	0.00	0.00	12	12	0	0	满足
223	0.0 6	0.06	0.06	0.00	0.00	0	0	0	0	满足
224	0.1 9	0.19	0.19	0.02	0.01	16	73	0	0	满足
225	0.1 6	0.16	0.16	0.05	0.01	0	0	0	0	满足
226	0.1 1	0.21	0.21	0.02	0.00	46	141	0	0	满足
227	0.0 2	0.02	0.02	0.16	0.05	0	0	0	0	满足
228	0.0 5	0.05	0.05	0.00	0.00	12	12	0	0	满足
229	0.0 5	0.05	0.05	0.00	0.00	0	0	0	0	满足
230	0.0 8	0.16	0.17	0.01	0.00	46	141	0	0	满足
231	0.0 2	0.02	0.02	0.19	0.02	0	0	0	0	满足
232	0.0 1	0.01	0.01	0.00	0.01	0	0	0	0	满足
233	0.0 2	0.05	0.04	0.01	0.00	12	53	1/312	0	满足
234	0.0 2	0.05	0.04	0.01	0.00	12	53	1/209	0	满足
235	0.0	0.05	0.04	0.01	0.00	12	53	1/339	1/607	满足

	2								09	
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最严控制表 (强度和整体稳定为(应力/设计强度))

	强度	绕2轴 整体稳定	绕3轴 整体稳定	绕2轴 抗剪应力比	绕3轴 抗剪应力比	绕2轴 长细比	绕3轴 长细比	绕2轴 W/1	绕3轴 W/1
所在单元	173	132	173	220	217	189	201	86	86
数值	0.56	0.57	0.56	0.20	0.07	91	172	1/144	1/262

“强度应力比”最大的前 10 个单元的验算结果 (所在组合号 / 情况号)

序号	单元号	强度	绕2轴 整体稳定	绕3轴 整体稳定	绕2轴 抗剪应力比	绕3轴 抗剪应力比	绕2轴 长细比	绕3轴 长细比	绕2轴 W/1	绕3轴 W/1	结果
1	173	0.56 (1/1)	0.56	0.56	0.00	0.00	8	8	1/33 82	0	满足
2	174	0.52 (4/1)	0.53	0.53	0.00	0.00	8	8	1/34 95	0	满足
3	176	0.52 (4/1)	0.52	0.52	0.07	0.02	9	39	0	0	满足
4	62	0.50 (1/1)	0.50	0.50	0.07	0.00	9	39	0	0	满足
5	42	0.46 (1/1)	0.46	0.46	0.07	0.00	9	39	0	0	满足
6	175	0.46 (1/1)	0.53	0.47	0.04	0.00	19	86	0	0	满足
7	81	0.44 (1/1)	0.45	0.45	0.00	0.00	8	8	1/47 78	0	满足
8	39	0.44 (1/1)	0.44	0.44	0.06	0.00	9	39	0	0	满足
9	80	0.43 (4/1)	0.43	0.43	0.00	0.00	8	8	1/48 06	0	满足
10	157	0.42 (1/1)	0.42	0.42	0.13	0.00	3	14	0	0	满足

按“强度应力比”统计结果表

范围	单元号	>1.05	1.05~1.00	1.00~0.80	0.80~0.60	0 · 6 0 ~ 0 · 0 0
单元数	0	0	0	0	235	

“绕2轴整体稳定应力比”最大的前 10 个单元的验算结果（所在组合号 / 情况号）

序号	单元号	强度	绕2轴 整体 稳定	绕3 轴 整体 稳定	绕2 轴 抗剪 应力 比	绕3 轴 抗剪 应力 比	绕2 轴 长细 比	绕3 轴 长细 比	绕2 轴 W/1	绕3 轴 W/1	结果
1	132	0.3 1	0.57 (4/1)	0.49	0.07	0.01	9	39	0	0	满足
2	60	0.2 1	0.57 (1/1)	0.48	0.16	0.01	3	14	0	0	满足
3	173	0.5 6	0.56 (1/1)	0.56	0.00	0.00	8	8	1/33 82	0	满足
4	174	0.5 2	0.53 (4/1)	0.53	0.00	0.00	8	8	1/34 95	0	满足
5	175	0.4 6	0.53 (1/1)	0.47	0.04	0.00	19	86	0	0	满足
6	40	0.1 7	0.53 (1/1)	0.44	0.14	0.01	3	14	0	0	满足
7	159	0.2 8	0.52 (4/1)	0.44	0.06	0.00	9	39	0	0	满足
8	142	0.2 7	0.52 (4/1)	0.44	0.06	0.00	9	39	0	0	满足
9	176	0.5 2	0.52 (4/1)	0.52	0.07	0.02	9	39	0	0	满足
10	37	0.1 7	0.51 (1/1)	0.42	0.14	0.00	3	14	0	0	满足

按“绕2轴整体稳定应力比”统计结果表

范围	单元号	>1.05	1.05~1.00	1.00~0.80	0.80~0.60	0 · 6 0 ~ 0 · 0 0
单元数	0	0	0	0	235	

“绕3轴整体稳定应力比”最大的前 10 个单元的验算结果（所在组合号 / 情况号）

序号	单元号	强度	绕2轴整体稳定	绕3轴整体稳定	绕2轴抗剪应力比	绕3轴抗剪应力比	绕2轴长细比	绕3轴长细比	绕2轴 W/1	绕3轴 W/1	结果
1	173	0.56	0.56	0.56 (1/1)	0.00	0.00	8	8	1/33 82	0	满足
2	174	0.52	0.53	0.53 (4/1)	0.00	0.00	8	8	1/34 95	0	满足
3	176	0.52	0.52	0.52 (4/1)	0.07	0.02	9	39	0	0	满足
4	62	0.50	0.50	0.50 (1/1)	0.07	0.00	9	39	0	0	满足
5	132	0.31	0.57	0.49 (4/1)	0.07	0.01	9	39	0	0	满足
6	65	0.41	0.41	0.49 (4/1)	0.02	0.03	33	9	0	0	满足
7	60	0.21	0.57	0.48 (1/1)	0.16	0.01	3	14	0	0	满足
8	175	0.46	0.53	0.47 (1/1)	0.04	0.00	19	86	0	0	满足
9	42	0.46	0.46	0.46 (1/1)	0.07	0.00	9	39	0	0	满足
10	81	0.44	0.45	0.45 (1/1)	0.00	0.00	8	8	1/47 78	0	满足

按“绕3轴整体稳定应力比”统计结果表

范围	单元号	>1.05	1.05~1.00	1.00~0.80	0.80~0.60	0 · 6 0 ~ 0 · 0 0
单元数	0	0	0	0	235	

“绕2轴长细比”最大的前 10 个单元的验算结果

序号	单元号	强度	绕2轴整体稳定	绕3轴整体稳定	绕2轴抗剪应力比	绕3轴抗剪应力比	绕2轴长细比	绕3轴长细比	绕2轴 W/1	绕3轴 W/1	结果
1	189	0.07	0.09	0.12	0.01	0.00	91	86	0	0	满足
2	199	0.23	0.23	0.41	0.02	0.01	48	53	0	0	满足
3	226	0.11	0.21	0.21	0.02	0.00	46	141	0	0	满足
4	230	0.08	0.16	0.17	0.01	0.00	46	141	0	0	满足
5	210	0.10	0.18	0.22	0.01	0.00	44	86	0	0	满足
6	211	0.00	0.00	0.00	0.00	0.00	44	3	1/50 3	0	满足
7	83	0.15	0.15	0.15	0.01	0.01	39	11	0	0	满足
8	84	0.08	0.08	0.08	0.01	0.00	39	11	0	0	满足
9	13	0.19	0.19	0.19	0.01	0.00	38	116	0	0	满足
10	120	0.13	0.13	0.13	0.01	0.00	38	116	0	0	满足

按“绕2轴长细比”统计结果表

范围	单元号	>180	180~150	150~120	120~80	8
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						0 ~ 0
单元数	0	0	0	1	234	

“绕3轴长细比”最大的前 10 个单元的验算结果

序号	单元号	强度	绕2轴整体稳定	绕3轴整体稳定	绕2轴抗剪应力比	绕3轴抗剪应力比	绕2轴长细比	绕3轴长细比	绕2轴 W/1	绕3轴 W/1	结果
1	201	0.19	0.19	0.19	0.01	0.00	33	172	0	0	满足
2	202	0.27	0.27	0.27	0.01	0.00	23	172	0	0	满足
3	203	0.12	0.19	0.36	0.01	0.00	33	172	0	0	满足
4	204	0.19	0.27	0.44	0.02	0.00	23	172	0	0	满足
5	207	0.22	0.22	0.22	0.01	0.00	31	166	0	0	满足
6	208	0.30	0.30	0.30	0.01	0.02	23	166	0	0	满足
7	205	0.15	0.21	0.38	0.01	0.00	31	166	0	0	满足
8	206	0.19	0.28	0.45	0.01	0.01	23	166	0	0	满足
9	226	0.11	0.21	0.21	0.02	0.00	46	141	0	0	满足
10	230	0.08	0.16	0.17	0.01	0.00	46	141	0	0	满足

按“绕3轴长细比”统计结果表

范围	单元号	>180	180~150	150~120	120~80	8 0 ~ 0
单元数	0	8	2	70	155	

基础JC-1计算书

项目名称：新工程一

基础部分

1 计算依据的规范和规程

- 1.1 《建筑地基基础设计规范》(GB 50007--2011)
- 1.2 《混凝土结构设计规范》(GB 50010--2011)
- 1.3 《建筑抗震设计规范》(GB 50011--2010)
- 1.4 《建筑结构荷载规范》(GB 50009--2012)

2 几何数据及材料

- 2.1 基础混凝土等级: C30; 抗压强度 $f_c=14.3$ (MPa); 抗拉强度 $f_t=1.43$ (MPa)
- 2.2 钢筋等级: HRB335; 强度设计值 $f_y=300$ (MPa); 纵筋合力点至近边距离 $a_s=50$ (mm)
- 2.3 基础类型: 锥型基础
- 2.4 基础长 $l=6000$ (mm); 基础宽 $b=6000$ (mm); 基础高 $h=3300$ (mm)
- 2.5 柱高 $H_c=450$ (mm); 柱宽 $B_c=450$ (mm);
柱周加大尺寸(相当于杯口厚度) $a_c=50$ (mm); 加大高度 $h_c=2400$ (mm)
- 2.6 基础端部高 $h_1=450$ (mm)
- 2.7 基础底面积 $A=l*b=6000*6000=36.000$ (m²)

$$\text{基础顶部面积 } A_t=(H_c+2*a_c)*(B_c+2*a_c)=(450+2*50)*(450+2*50)=0.302(\text{m}^2)$$

$$\begin{aligned} \text{基础体积 } V_{jc}= & l*b*h_1+[(B_c+2*a_c)*(H_c+2*a_c)+(l-H_c-2*a_c)*(b-B_c-2*a_c)]/3 \\ & + (l-H_c-2*a_c)*(B_c+2*a_c)/2+(b-B_c-2*a_c)*(H_c+2*a_c)/2]* (h-h_1-h_c) \\ & + (H_c+2*a_c)*(B_c+2*a_c)*h_c \end{aligned}$$

$$=6000*6000*450+[(450+2*50)*(450+2*50)+(6000-450-2*50)*(6000-450-2*50)]/3$$

$$\begin{aligned} & + (6000-450-2*50)*(450+2*50)/2+(6000-450-2*50)*(450+2*50)/2]* (3300-450-2400) \\ & + (450+2*50)*(450+2*50)*2400 \\ & =22.866(\text{m}^3) \end{aligned}$$

2.8 基础自重和上部土重

$$\text{基础混凝土的容重 } \gamma_c=25.00(\text{kN}/\text{m}^3)$$

$$\text{基础顶面以上土的容重 } \gamma_s=18(\text{kN}/\text{m}^3)$$

$$\text{基础及以上土重 } G_k=V_{jc}*\gamma_c+[A*d-V_{jc}-B_c*H_c*(d-h)]*\gamma_s$$

$$=22.866*25.0+[36.000*3.800-22.866-0.450*0.450*(3.800-3.300)]*18$$

$$=2620.642(\text{kN})$$

$$G=1.2*G_k=3144.771(\text{kN})$$

3 地基承载力信息

3.1 已知条件

$$\text{地基承载力特征值 } f_{ak}=120(\text{kPa})$$

$$\text{当地震参与荷载组合时地耐力提高系数 } \xi_a=1$$

$$\text{宽度修正系数 } \eta_b=0; \text{ 深度修正系数 } \eta_d=1$$

$$\text{土的重度 } \gamma=18(\text{kN}/\text{m}^3); \text{ 土的加权平均重度 } \gamma_m=20(\text{kN}/\text{m}^3)$$

$$\text{基础短边尺寸 } b=6000(\text{mm}); \text{ 基础埋置深度 } d=3800(\text{mm}); \text{ 深度修正起算深度 } d_1=0(\text{mm})$$

3.2 承载力设计值

$$f_a=f_{ak}+\eta_b*\gamma*(b-3)+\eta_d*\gamma_m*(d-d_1-0.5) \quad (\text{GB 50007--2002 式5.2.4, 按北京规范可把}d_1\text{加大1m})$$

$$f_a=120+0*18*(6-3)+1*20*(3.8-0-0.5)=186.000(\text{kPa})$$

$$f_aE=\xi_a*f_a \quad (\text{GB 50011--2001 式4.2.3})$$

$$f_aE=1*186.000=186.000(\text{kPa})$$

3.3 基底允许出现零应力区占基底总面积的百分比: 0%

4 荷载信息

4.1 符号说明:

N 、 N_k ----- 柱底轴向力设计值、标准值(kN)
 F 、 F_k ----- 作用于基础顶面的竖向力设计值、标准值(kN)
 Q 、 Q_k ----- 作用于地面的附加地面堆载设计值、标准值(kN/m²)
 F_x' 、 F_y' 、 F_{kx}' 、 F_{ky}' ----- 作用于基础顶面的附加荷载设计值、标准值(kN)
 $F_x'=0$; $F_y'=0$; $Q=0$; 地面堆载按活荷载考虑(考虑最不利情况)
 a_x' 、 a_y' ----- 作用于基础顶面的附加荷载偏心(mm)
 $a_x'=0$; $a_y'=0$
 V_x 、 V_y ---- 作用于基础顶面的剪力设计值(kN)
 V_{kx} 、 V_{ky} ---- 作用于基础顶面的剪力标准值(kN)
 M_x' 、 M_y' ---- 作用于基础顶面的弯矩设计值(kN*m)
 M_{kx}' 、 M_{ky}' ---- 作用于基础顶面的弯矩标准值(kN*m)
 M_{kx} 、 M_{ky} ---- 作用于基础底面的弯矩标准值(kN*m)
 γ_z ----- 荷载设计值换算为标准值的折减系数

$$\gamma_z=1.3$$

$$F_k=N_k+F_{kx}'+F_{ky}'$$

$$M_{kx}=M_x'-V_{ky}*H-F_{ky}'*a_y'$$
, $M_{ky}=M_y'+V_{kx}*H+F_{kx}'*a_x'$

$$F_k=F/\gamma_z$$
, $M_{kx}'=M_x/\gamma_z$, $M_{ky}'=M_y/\gamma_z$

4.2 直接输入荷载设计值

$$N=1200$$
; $M_x=115$; $M_y=113$; $V_x=211$; $V_y=125$

$$F_k=(N+F_x'+F_y')/\gamma_z=(1200+0+0)/1.3=923.077$$
 (kN)

$$M_{kx}=(M_x'-V_y*H-F_y'*a_y')/\gamma_z=(115-125*3.3-0*0)/1.3=-228.846$$
 (kN*m)

$$M_{ky}=(M_y'+V_x*H+F_x'*a_x')/\gamma_z=(113+211*3.3+0*0)/1.3=622.538$$
 (kN*m)

5 轴心荷载作用下验算

$$p_k=(F_k+G_k+Q_k)/A$$
 (GB 50007--2002 式5.2.2-1)

$$p_k=(923.077+2620.642+0.000)/36.000=98.437$$
 (kPa) ≤ 186.000 满足要求

6 偏心荷载作用下验算

单向偏心荷载作用下公式

$$p_{kmax}=(F_k+G_k+Q_k)/A+M_k/W$$
 (GB 50007--2002 式5.2.2-2)

$$p_{kmin}=(F_k+G_k+Q_k)/A-M_k/W$$
 (GB 50007--2002 式5.2.2-3)

当基底出现拉力区时, $p_{kmax}=2*(F_k+G_k)/1/a/3$ (GB 50007--2002 式5.2.2-4)

双向偏心荷载作用下公式

$$p_{kmax}=(F_k+G_k+Q_k)/A+M_{kx}/W_x+M_{ky}/W_y$$

$$p_{kmin}=(F_k+G_k+Q_k)/A-M_{kx}/W_x-M_{ky}/W_y$$

当基底出现拉力区时, p_{kmax} 按与 $F_k+G_k+Q_k$ 等值原则进行修正

$$\text{基础底面抵抗矩 } W_x=1*b*b/6=6000*6000*6000/6=36.000$$
 (m³)

$$W_y=b*1*1/6=6000*6000*6000/6=36.000$$
 (m³)

$$p_{kmax}=(923.077+2620.642+0.000)/36.000+228.846/36.000+622.538/36.000$$

$$=115.729$$
 (kPa) $\leq 1.2*186.000=223.200$ (kPa) 满足要求

$$p_{kmin}=(F_k+G_k+Q_k)/A-M_{kx}/W_x-M_{ky}/W_y$$

$$p_{kmin}=(923.077+2620.642+0.000)/36.000-228.846/36.000-622.538/36.000$$

$$=74.787$$
 (kPa)

出现拉应力区面积占基底面积百分比=0.000% ≤ 0.000% 满足要求
 偏心矩 $e_x = M_k y / (F_k + G_k) = 622.538 / (923.077 + 2620.642 + 0.176) = 0.000$ (m)
 $e_y = M_k x / (F_k + G_k) = -228.846 / (923.077 + 2620.642) = -0.065$ (m)

7 基础冲切验算

$F_l \gamma_{RE} \leq 0.7 \beta_{hp} f_t a_m h_0$ (GB 50007--2002 式8.2.7-1)
 γ_{RE} --承载力抗震调整系数, 当有地震参与时取0.85, 其它取1.0
 $h_0 = h - a_s$
 $a_m = (a_x + a_y) / 2$ (GB 50007--2002 式8.2.7-2)
 $a_{bx} = \text{Min}(l, a_x + 2h_0)$
 $a_{by} = \text{Min}(b, a_y + 2h_0)$
 $F_l = p_j A_l$ (GB 50007--2002 式 8.2.7-3)
 $A_{lx} = (b - a_{by}) * l / 2 - (1 - a_{bx}) * (1 - a_{bx}) / 4$
 $A_{ly} = (l - a_{bx}) * b / 2 - (b - a_{by}) * (b - a_{by}) / 4$
 $p_j = \gamma_z * (P_{kmax} - G_k / A)$

7.1 柱底边冲切面验算

$\beta_{hp} = 0.90$; $h_0 = 3.25$ (mm)
 $a_{tx} = H_c = 0.45$ (m); $a_{bx} = 6$ (m); $a_{mx} = 3.225$ (m)
 $a_{ty} = B_c = 0.45$ (m); $a_{by} = 6$ (m); $a_{my} = 3.225$ (m)
 $A_{lx} = 0$ (m²); $A_{ly} = 0$ (m²)
 $p_j = 1.3 * (115.729 - 2620.642 / 36.000) = 55.814$ (kPa)
 $F_{lx} \gamma_{RE} = 55.814 * 0.000 * 0.85 = 0.000$ (kN) ≤ 9442.558 (kN) 满足要求
 $F_{ly} \gamma_{RE} = 55.814 * 0.000 * 0.85 = 0.000$ (kN) ≤ 9442.558 (kN) 满足要求

7.2 柱周加大底边(基础顶)冲切面验算

$\beta_{hp} = 0.99$; $h_0 = 0.85$ (mm)
 $a_{tx} = H_c = 0.55$ (m); $a_{bx} = 2.25$ (m); $a_{mx} = 1.4$ (m)
 $a_{ty} = B_c = 0.55$ (m); $a_{by} = 2.25$ (m); $a_{my} = 1.4$ (m)
 $A_{lx} = 7.73438$ (m²); $A_{ly} = 7.73438$ (m²)
 $p_j = 1.3 * 115.729 - 2620.642 / 36.000 = 55.814$ (kPa)
 $F_{lx} \gamma_{RE} = 55.814 * 7.734 * 0.85 = 366.933$ (kN) ≤ 1181.263 (kN) 满足要求
 $F_{ly} \gamma_{RE} = 55.814 * 7.734 * 0.85 = 366.933$ (kN) ≤ 1181.263 (kN) 满足要求

8 柱下局部受压承载力验算

$F_l \leq \omega * \beta_l * f_{cc} * A_l$ (GB 50010--2002 式A.5.1-1)
 $F_l = 1200$ (kN)
 $f_{cc} = 0.85 * f_c$
 混凝土局部受压面积 $A_l = B_c * H_c = 0.45 * 0.45 = 0.202$ (m²)
 局部受压时的计算底面积 $A_b = (H_c + 2 * c) * (B_c + 2 * c) = 0.3025$ (m²)
 $\beta_l = \text{Sqrt}(A_b / A_l) = \text{Sqr}(0.302 / 0.202) = 1.222$
 $\omega * \beta_l * f_{cc} * A_l = 1.0 * 1.222 * 0.85 * 14.300 * 0.202 = 3008.363$ (kN)
 $\geq F_l = 1200.000$ (kN) 满足要求

9 抗弯计算

$M_I = a_l^2 * [(2 * l + a') * (p_{max} + p - 2 * G / A) + (p_{max} - p) * l] / 12 * \gamma_{RE}$ (GB 50007--2002 式8.2.7-4)

$= a_l^2 * [(2 * l + a') * (P_{jmax} + p_j) + (P_{jmax} - p_j) * l] / 12 * \gamma_{RE}$
 $M_{II} = (1 - a')^2 * (2 * b + b') * (p_{max} + p_{min} - 2 * G / A) / 48 * \gamma_{RE}$ (GB 50007--2002 式8.2.7-5)

$$=(1-a')^2 \cdot (2b+b') \cdot (P_{jmax}+P_{jmin}) / 48 \cdot \gamma_{RE}$$

γ_{RE} --承载力抗震调整系数, 当有地震参与时取0.75, 其它取1.0

9.1 柱边弯矩计算

9.1.1 绕Y轴方向弯矩计算:

$$l=6.000(m); a'=0.450(m); a_1=2.775(m)$$

$$P_{jmax}=64.078(kPa); P_{jmin}=-5.103(kPa)$$

$$p_j=P_{jmax}-(P_{jmax}-P_{jmin}) \cdot a_1 / l=45.485(kPa)$$

$$M_I = a_1^2 \cdot [(2 \cdot 1 + a') \cdot (P_{jmax} + p_j) + (P_{jmax} - p_j) \cdot 1] / 12 \cdot \gamma_{RE}$$

$$= 2.775^2 \cdot [(2 \cdot 6.000 + 0.450) \cdot (64.078 + 45.485) + (64.078 - 45.485) \cdot 6.000] / 12 \cdot 0.75$$

$$= 710.198(kN \cdot m)$$

截面面积A=5.494(m²), 受压区高度x=0.028(m)

As=720.404(mm²); 配筋率 $\rho = 0.01\%$

9.1.2 绕X轴方向弯矩计算:

$$l=6.000(m); a'=0.450(m); a_1=2.775(m)$$

$$P_{jmax}=64.078(kPa); P_{jmin}=-5.103(kPa)$$

$$P_j=P_{jmax}-(P_{jmax}-P_{jmin}) \cdot a_1 / l=45.485(kPa)$$

$$M_I = a_1^2 \cdot [(2 \cdot 1 + a') \cdot (P_{jmax} + p_j) + (P_{jmax} - p_j) \cdot 1] / 12 \cdot \gamma_{RE}$$

$$= 2.775^2 \cdot [(2 \cdot 6.000 + 0.450) \cdot (64.078 + 45.485) + (64.078 - 45.485) \cdot 6.000] / 12 \cdot 0.75$$

$$= 710.198(kN \cdot m)$$

截面面积A=5.494(m²), 受压区高度x=0.028(m)

As=720.404(mm²); 配筋率 $\rho = 0.01\%$

9.2 柱周加大底边(基础顶)弯矩计算

9.2.1 绕Y轴方向弯矩计算:

$$l=6.000(m); a'=0.550(m); a_1=2.725(m)$$

$$P_{jmax}=64.078(kPa); P_{jmin}=-5.103(kPa)$$

$$p_j=P_{jmax}-(P_{jmax}-P_{jmin}) \cdot a_1 / l=45.197(kPa)$$

$$M_I = a_1^2 \cdot [(2 \cdot 1 + a') \cdot (P_{jmax} + p_j) + (P_{jmax} - p_j) \cdot 1] / 12 \cdot \gamma_{RE}$$

$$= 2.725^2 \cdot [(2 \cdot 6.000 + 0.550) \cdot (64.078 + 45.197) + (64.078 - 45.197) \cdot 6.000] / 12 \cdot 0.75$$

$$= 689.044(kN \cdot m)$$

截面面积A=4.174(m²), 受压区高度x=0.061(m)

As=2654.879(mm²); 配筋率 $\rho = 0.06\%$

控制最小配筋率 $\rho_{min} = 0.15\%$; As=6260.625(mm²)

9.2.2 绕X轴方向弯矩计算:

$$l=6.000(m); a'=0.550(m); a_1=2.725(m)$$

$$P_{jmax}=64.078(kPa); P_{jmin}=-5.103(kPa)$$

$$P_j=P_{jmax}-(P_{jmax}-P_{jmin}) \cdot a_1 / l=45.197(kPa)$$

$$M_I = a_1^2 \cdot [(2 \cdot 1 + a') \cdot (P_{jmax} + p_j) + (P_{jmax} - p_j) \cdot 1] / 12 \cdot \gamma_{RE}$$

$$= 2.725^2 \cdot [(2 \cdot 6.000 + 0.550) \cdot (64.078 + 45.197) + (64.078 - 45.197) \cdot 6.000] / 12 \cdot 0.75$$

$$= 689.044(kN \cdot m)$$

截面面积A=4.174(m²), 受压区高度x=0.061(m)

As=2654.879(mm²); 配筋率 $\rho = 0.06\%$

控制最小配筋率 $\rho_{min} = 0.15\%$; As=6260.625(mm²), Ax=3.94234e-281

9.3 配筋结果:

沿X向钢筋 $A_s=6260.625$ (mm²); 实配 $\phi 16@150$ ($A_s=6898.937$)
沿Y向钢筋 $A_s=6260.625$ (mm²); 实配 $\phi 16@150$ ($A_s=6898.937$)

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